

Avonbank Heavy Mineral Sands Project WIM Resource Pty Ltd 06-Jun-2019 Doc No. 60595006-ENV-RPT-002

2019 Hydrogeology Summary Report

Avonbank Heavy Mineral Sands Project

2019 Hydrogeology Summary Report

Avonbank Heavy Mineral Sands Project

Client: WIM Resource Pty Ltd

ABN: 59159389929

Prepared by

AECOM Australia Pty Ltd Level 10, Tower Two, 727 Collins Street, Melbourne VIC 3008, Australia T +61 3 9653 1234 F +61 3 9654 7117 www.aecom.com ABN 20 093 846 925

06-Jun-2019

Job No.: 60595006

AECOM in Australia and New Zealand is certified to ISO9001, ISO14001 AS/NZS4801 and OHSAS18001.

© AECOM Australia Pty Ltd (AECOM). All rights reserved.

AECOM has prepared this document for the sole use of the Client and for a specific purpose, each as expressly stated in the document. No other party should rely on this document without the prior written consent of AECOM. AECOM undertakes no duty, nor accepts any responsibility, to any third party who may rely upon or use this document. This document has been prepared based on the Client's description of its requirements and AECOM's experience, having regard to assumptions that AECOM can reasonably be expected to make in accordance with sound professional principles. AECOM may also have relied upon information provided by the Client and other third parties to prepare this document, some of which may not have been verified. Subject to the above conditions, this document may be transmitted, reproduced or disseminated only in its entirety.

Quality Information

Document 2019 Hydrogeology Summary Report

Ref 60595006

Date 06-Jun-2019

Prepared by Timothy Smith

Reviewed by Bryan Chadwick

Revision History

Rev	Revision Date	Details	Authorised				
1.00			Name/Position	Signature			
4	06-June-2019	Final	Timothy Smith Project Manager	Al			

Table of Contents

Executiv	e Summa	ıry			i
1.0	Introduct				1
	1.1	Project	Background		1
	1.2	Scope of	of work		2
		1.2.1	Hydrogeological Critical Review		2 2 2 4
		1.2.2	Field Investigations		2
2.0	Site Sett				
	2.1		stratigraphy		4
		2.1.1	Quaternary Aquifer (QA)		4
		2.1.2	Upper Tertiary Aquifer (fluvial) (UTAF)		4
		2.1.3	Upper Tertiary Aquifer (marine) (UTAM)		4
		2.1.4	Upper Tertiary Aquitard (UTD)		5 5
		2.1.5	Lower Tertiary Aquifer (LTA)		5
		2.1.6	Mesozoic and Palaeozoic Bedrock (BSE)		6
	2.2		water Levels and Flow Direction		1
		2.2.1	UTAM/QA		1
		2.2.2	LTA		1
		2.2.3	Vertical Gradients		1
	~ ~	2.2.4	Connectivity between LTA and UTAM/QA		2
	2.3		water quality		3
		2.3.1	Salinity Major Jone		ა ე
2.0	Discussi	2.3.2	Major Ions		233355556
3.0	Discussi	-	Water Croundwater Interaction		0
	3.1	3.1.1	Water – Groundwater Interaction Water Courses and Water Bodies		о г
		3.1.1	Dooen Swamp		5
		3.1.2	Darlot Swamp		ິດ
		3.1.3	Yarriambiack Creek and Two Mile Creek		6
4.0	Conclusi		Tarriandiack Creek and Two Mile Creek		8
4 .0 5.0	Limitatio				9
6.0	Reference			1	
0.0	I CICICIII	563		I	0
Appendi					
	Figures				A
Appendi	хВ				
, ipportai	Tables				B
Appendi					~
	Bore Log	js		(С
Appendi	хD				
		vater Lab	ooratory Analysis Reports	I	D

WIM Resource Pty Ltd (WIM) is currently progressing mining feasibility investigations at their Avonbank Heavy Mineral Sands Mine which is within Retention Licence 2014 (RL2014), located near Horsham in Western Victoria.

The key objective of this report is to provide an updated understanding of the baseline hydrogeology, specifically focused on the potential for and risks to Groundwater Dependant Ecosystems (GDE) in proximity to the Project.

WIM engaged AECOM Australia Pty Ltd (AECOM) to undertake a critical review of hydrogeological studies conducted to date and identify any potential data gaps in the conceptual hydrogeological understanding. Outcomes of the critical review highlighted:

- The need to further understand surface water groundwater interactions in nearby ephemeral surface water features (Dooen Swamp, Darlot Swamp, Yarriambiack Creek and Two Mile Creek); and
- The need to further understand hydraulic connectivity between the Upper Tertiary (marine) Aquifer (UTAM), present within the Loxton Parilla Sands, and the Lower Tertiary Aquifer (LTA), which is present within the Renmark Group.

To address these data gaps works a program of air core drilling and groundwater bore drilling and additional groundwater monitoring bore installations were completed in early 2019.

The factual conclusions of 2019 site investigations were as follows:

- The upper aquifer (UTAM) beneath the Mine is brackish (salinity generally 6,000 to 13,000 mg/L TDS) with limited users in the vicinity of the mine plan area (only two registered stock and domestic bores within a 5 km radius).
- Groundwater within the upper aquifer shows a general increase in salinity down flow path (northwards), away from the surface drainage features present south of the proposed Mine.
- There is little change in hydro-geochemistry between up-gradient bores (south), bores adjacent to surface drainage features, bores screened within the mineralised zone and down gradient outside of the mineralised zone (north).
- Geera Clay is found to consist of a high plasticity clay unit beneath entire Mine site, with an observed head difference between the overlying (UTAM) and underlying (LTA) aquifers where monitored.
- The depth to groundwater beneath the lowest points of Darlot and Dooen Swamps is greater than 5 metres (measured in March 2019 at 5.9 and 6.2m respectively).
- Downward vertical gradient immediately adjacent to swamps.

The implications of this updated factual information on the groundwater risks from the Project are as follows:

- The ephemeral swamps (Dooen and Darlot) are losing systems, whereby they recharge the underlying aquifer whenever they fill with surface water flows.
- The depth to groundwater, vertical hydraulic gradient and groundwater salinity profile indicates that within Dooen Swamp and Darlot Swamp there is:
 - no potential for aquatic GDEs;
 - potential for terrestrial GDEs, but only if there exists deep rooted (phreatophyte) type vegetation that requires more than periodic flooding and is tolerant to brackish water.
- The mining of the mineral sands within the project area will require dewatering the upper aquifer (UTAM) by less than 10 metres. The extent of the resultant cone of depression will be limited by the relatively low permeability and temporal period of dewatering.

- Any tailings disposal into the mining voids will result in seepage of water entering the upper aquifer system, and will result in some level of mounding and changes to groundwater quality. The brackish nature and limited users of the upper aquifer (UTAM) across the Mine footprint mean the consequences are likely to be minor.
- Limited risks to the underlying Renmark Group aquifer (LTA) from either dewatering or mounding in the upper aquifer (UTAM) given the nature and occurrence of the mapped Geera Clay aquitard.

1.0 Introduction

1.1 Project Background

WIM Resource Pty Ltd (WIM) is progressing mining feasibility investigations at their Avonbank Heavy Mineral Sands Project ('Mine'). The proposed Mine is within, and covers less 40 percent of Retention Licence 2014 (RL2014), which is located near Horsham in Western Victoria (shown in

Figure 1, Appendix A).

The key objective of this report is to provide an updated understanding of the hydrogeology, specifically focused on the potential for Groundwater Dependant Ecosystems (GDE) in proximity to the Mine, based on field works undertaken in early 2019.

1.2 Scope of work

1.2.1 Hydrogeological Critical Review

In December 2018, WIM engaged AECOM Australia Pty Ltd (AECOM) to undertake a critical review of hydrogeological studies conducted to date. Outcomes of the review identified a number of data gaps in the conceptual hydrogeological understanding. To address these gaps, further drilling investigations and additional groundwater monitoring bore installations were proposed.

The critical review collated all available information, including previous investigations, with the intention to identify key data gaps that need to be addressed in preparation of the bulk test pit program and any EES submissions. The reports included in the review were:

- 1. Avonbank HMS Project Desktop Hydrogeological Assessment, prepared by GHD, August 2018.
- Avonbank HMS project Groundwater monitoring bore and aquifer testing completion report, prepared by GHD, August 2018.
- 3. Groundwater Modelling Results, prepared by GHD, October 2018.
- 4. Report on Geotechnical Drilling Program, Preliminary Assessment of Pit Slopes, Trafficability and Excavabaility. Report no: 115138.01, prepared by ATC Williams, June 2017.
- 5. Warracknabeal and Brim Flood Investigation Hydrology and Hydraulics. Prepared for Wimmera Catchment Management Authority by Water Technology, 2015.

1.2.2 Field Investigations

In February 2019, field groundwater based investigations were undertaken as recommended in the hydrogeological review. This work included:

1. Installation of six additional groundwater monitoring bores (GW18, GW19, GW20, GW21 and GW22) (locations shown on

- 2.
- 3. Figure 1, Appendix A construction detail provided in Table 1, Appendix B); and
- 4. Groundwater monitoring event of key bores (GW05, GW14, GW18, GW19, GW21 and GW22);
 - Sampling of groundwater bores was completed using low flow techniques in accordance with the groundwater sampling guidelines- EPA publication 669 (EPA, 2000);
 - Groundwater bores standing water level and total bore depths were measured prior to any sampling or installation of sampling equipment;
 - Measurement of field parameters- Electrical Conductivity, pH, temperature and redox during sampling was recorded to ensure collection of a representative groundwater sample;
 - Field Quality Assurance and Quality Control (QA/QC) samples were collected to ensure sampling and lab analysis techniques are adequate;
 - Water quality samples were sent to a NATA accredited laboratory and tested for the following laboratory analytical suite;
 - Salinity (as EC, as TDS);
 - Alkalinity (Total, OH, HCO₃, CO₃, Hardness);
 - Major lons (Na, Ca, K, Mg, Cl, SO₄);
 - Metals (Al, As, Ba, Be, Br, B, Cd, Ce, Cr, Co, Cu, Fe, Pb, Mn, Hg, Mo, Ni, Se, Ag, Sr, Tl, Sn, Ti, V, Y, Zn);
 - Radionuclides (including gross alpha and beta) (bores GW05, GW20 and GW21 only), and
 - Uranium and Thorium (bores GW05, GW20 and GW21 only).
- 5. Deployment of electronic groundwater level data loggers in key bores recording on a daily interval.

2.0 Site Setting

A detailed regional outline of the hydrogeological setting of the Mine is provided in the Avonbank Hydrogeological Assessment (GHD, 2018). The following is a summary of the key aspects updated based on the information and data collected from the field investigations outlined in Section 1.2.2 (above):

2.1 Hydro-stratigraphy

The Mine is located on the southern boundary of the Murray Basin, which has been filled with Tertiary aged marine and non-marine sediments. These are overlain in many locations by Quaternary aged aeolian, fluvial and lacustrine sediments.

A description of the geological stratigraphy and their associated hydrogeological units are provided Table 1. Detailed description of the stratigraphic units is provided below.

2.1.1 Quaternary Aquifer (QA)

The recent and Quaternary aged unconsolidated deposits (QA) associated with drainage lines are generally less than 10 m thick, and may be periodically saturated closer to drainages.

The QA may exist adjacent to drainages such as the Wimmera River to the south where the Loxton Parilla Sands (LPS) have been eroded allowing for channel infill of more recent sediments. Recent drilling results at GW22 to the south west of the Mine and GW18 to the south east of the mine indicated the LPS was absent and that recent fluvio-deltaic sediments directly overlie the Geera Clay and form the upper aquifer.

Recharge to the QA is anticipated via river systems (such as the Wimmera River) and other surface water bodies. Recharge is expected to largely occur during episodic flooding events which allow for recharge to the bank storage and adjacent sediments, eventually feeding seeping down into the underlying aquifer system.

2.1.2 Upper Tertiary Aquifer (fluvial) (UTAF)

The Tertiary aged Shepparton Formation sediments (UTAF) are not saturated within the Mine and its immediate surrounds, and thus do not form an aquifer unit to be considered.

2.1.3 Upper Tertiary Aquifer (marine) (UTAM)

The Loxton Parilla Sands, which host the Upper Tertiary aged aquifer (UTAM), is comprised of dune, foreshore or surf zone sands overlying the mineralised offshore sands. The LPS thickness has been found to range from 20 to 30 m across the Project site. The UTAM is associated with the lower portion of the Loxton Parilla Sands (LPS) and has been found to be less than 10 m in saturated thickness across the Mine.

Individual bore yields from the UTAM are expected to be less than 0.5 L/second as the sediments are typically dominated by clays and silts in this region and have a relatively low permeability in comparison to other areas further west of the Wimmera River. Hydraulic conductivity is reportedly to range from 0.01 to 5.3 m/day but is known to be higher in places outside the Project area (URS, 2010). Aquifer (slug) tests were completed in 2018 on the Avonbank project bores (GHD, 2018b), with results reported hydraulic conductivity ranging from 0.1 to 2.3 m/day.

Groundwater recharge is expected to occur on the floodplains via direct rainfall infiltration and through seasonal deep drainage. Low rainfall and high evaporation rates are expected to result in low recharge rates to the water table aquifer. Localised recharge may also occur in areas where the UTAM has a relatively high permeability.

From a groundwater flow system viewpoint, the UTAM and the adjacent QA are considered to be fully connected and essentially form a continuous aquifer unit and are referenced as the UTAM/QA throughout the remainder of this report.

2.1.4 Upper Tertiary Aquitard (UTD)

The Geera Clay forms the Upper Tertiary Aquitard (UTD) within the Murray Basin. It is a hydraulically confining unit separating the UTAM/QA from the deeper Renmark Group (Lower Tertiary Aquifer - LTA).

Resource drilling has confirmed the Geera Clay is beneath the entire Mine footprint and immediate surrounds.

Regionally, the Geera Clay is described as comprising silty sandy clays, sometimes pyritic and carbonaceous and often containing fossils. At the Mine, drilling results indicate the Geera Clays to be dominantly a high plasticity, silty-sandy, clay.

Across the broader region the Geera Clay is intercepted immediately below the LPS and is reported to be 20 to 40 m thick (GHD, 2018a). Project specific mapping of the Geera Clay suggests actual thickness increases from south east to north west (URS, 2010), with 2019 (air-core) drilling results completed by WIM confirming the Geera Clay thickness to be 13 m at GW18, adjacent to Darlot Swamp, and >40 m beneath the mineralised portions of the LPS (WIM, 2019).

2.1.5 Lower Tertiary Aquifer (LTA)

The Renmark Group sediments form the basal depositional sequence of the Murray Basin and comprise fluvio-lacustrine sediments which make up the Lower Tertiary Aquifer (LTA).

The Renmark Group is noted to be present at a depth of around 70 to 80 m where investigated within RL2014.

The thickness of the LTA is varying and is largely controlled by the undulating nature of the top of basement bedrock. Previous work done in the region has shown thickness between 34 and 75 m beneath the Mine (URS, 2010). The aquifer is noted to be thicker towards the north-west, and possibly absent to the east of the Mine.

Inspection of registered bore lithology (Bores ID 68429 and 68430 shown on

6

Figure 1, **Appendix A**) indicate the LTA thickness is >50 m in the south west corner of RL2014 at bore 68429 and possibly absent registered bore 68430, east of the site and adjacent to Yarriambiack Creek, which is consistent with the literature.

Aquifer yields can be highly variable and are generally expected to range from <5 to 5 L/sec (URS, 2010). Yields are expected to generally improve to the north-west where the aquifer system is deeper and thicker.

Overall, the nature and extent of the overlying Geera Clay (UTD) suggests that the LTA will be hydraulically isolated from impacts within the upper aquifer(s).

2.1.6 Mesozoic and Palaeozoic Bedrock (BSE)

The Murray Basin Bedrock Aquifer (BSE) consists of predominantly of Grampians Group marine and fluvial sandstone, siltstone and minor conglomerate, Moralana Supergroup marine sandstone and siltstone and unnamed Cambrain 'greenstone'.

Bedrock outcrops to the south (24 km) of the Mine in the Grampians Ranges and acts as primary recharge areas to the fractured bedrock aquifer and LTA. However, typically the BSE is highly weathered and clay dominant across is upper profile beneath the Murray Basin sediments (URS, 2010).

The significance of the BSE with respect to the Mine is considered negligible given its depth, upper weathering profile and the occurrence of the overlying Geera Clay aquitard. As such, the BSE is not discussed further.

Table 1 Stratigraphy

Period	Geological Unit	Geological Description	Location and Extent	Aquifer Unit ¹	Salinity (as TDS) range (mg/L)
Quaternary	Alluvial and Colluvial Deposits	Undifferentiated deposits of silty clays, sands and gravels	Outcropping along drainage lines (Yarriambiack Creek, Two Mile Creek and Wimmera River). Expected to be <10 m thick.	Quaternary Aquifer (QA)	Unknown
Quaternary/T ertiary (upper)	Formationlacustrine sediments consisting of sands, gravelsProject area. Generally <10 m thick across Project area.Tert (flux)		Quaternary / Upper Tertiary Aquifer (fluvial) (UTAF) <i>Not present</i>	Unknown	
Tertiary (upper)	Loxton Parilla Sands	Sands, sandstones and silt. Shallow marine deposit.	Regionally extensive unit. In the order of 20-30 m thick across Project site. Host unit to HMS orebody.	Upper Tertiary Aquifer (marine) (UTAM)	3,501 – 13,000
Tertiary	Geera Clay	Clay, dark grey-black rare silt, sometime glauconitic			Unknown
Tertiary	Renmark Group	Sands, gravels, clays	Regionally extensive but absent in local areas to the north east of the site	Lower Tertiary Aquifer (LTA)	3,501 – 13,000
Silurian	Grampians Group	Sandstones / siltstones / minor mudstones	Basement rock	Mesozoic and Palaeozoic Bedrock (BSE)	1,001 – 3,501

¹ Aquifer nomenclature based on the Victorian Aquifer Framework (DSE, 2012)

2.2 Groundwater Levels and Flow Direction

Groundwater levels have been measured monthly at all bores across the site since November 2018. Groundwater monitoring and elevation data is presented in **Table 3 and Table 4, Appendix B**.

2.2.1 UTAM/QA

The groundwater levels observed in the UTAM and QA (where present) ranged from 6.4 mbgl (GW19) to 37.9 mbgl (GW20) over the monitored period (November 2018 to May 2019).

The general pattern beneath the Mine is of an increasing depth to water from south to north. The saturated thickness of the UTAM is variable and appears to decrease along the observed flow path, to the northwest.

Depth to water plotted vs time (**Figure 4**, **Appendix A**) shows very little variation over the 7 month period and does not appear to be strongly influenced by seasonal variation. It is expected that water levels would be at annual maximums in November at the end of winter / spring season, then declining over the summer and autumn months.

It should be noted that measurements over the winter / spring higher rainfall months is absent from the dataset. In January 2019 the water level record at GW04 appears to be an outlier.

Interpolated groundwater flow contours (based on March 2019 data) in the UTAM/QA are presented in **Figure 3**, **Appendix A**. Groundwater elevations (plotted in **Figure 6**, **Appendix A**) range from 103 mAHD (GW20) to 126 mAHD (GW19) from southeast to northwest. The groundwater flow direction reflects topographic fall, in a north-north westerly direction. Measured groundwater elevation and flow direction at the project site are consistent with the regional publically available groundwater data as presented in the Desktop Hydrogeological Assessment (GHD, 2018a).

2.2.2 LTA

Groundwater in the LTA is confined, with groundwater levels in bores screened beneath the Geera Clay ranging between 5.8 mbgl (INV01) to 38.9 mbgl (GW10) (plotted in **Figure 5, Appendix A**). Similar to the UTAM there appears to be a general increasing depth to groundwater trend from south to north across the project site.

Groundwater elevations range from 107.2 mAHD (GW10) to 126.9 mAHD (INV01) (plotted in **Figure** 7, **Appendix A**). Similarly to the water table aquifer, groundwater flow direction in the LTA is northwards. Measured site data is consistent with the regional publically available groundwater data as presented in the Desktop Hydrogeological Assessment (GHD, 2018a).

2.2.3 Vertical Gradients

An indication of the vertical hydraulic gradient beneath the Darlot Swamp (located approximately 1.9 km from the Mine) can be estimated within the UTAM/QA and also compared with the underlying LTA. In this area three bores are screened at different intervals:

- GW18 is screened at the water table;
- GW14 is screened at the base of the UTAM/QA; and
- INV02 is screened in the confined LTA. A generalised schematic of the groundwater heads at various depths is presented in **Figure 9**, **Appendix A**.

Comparison of the levels in these three bores (based on November 2018 to May 2019 gauge results) shows the following:

- UTAM/QA A downward hydraulic gradient within the UTAM/QA of 0.015 m/m. This provides evidence that the ephemeral water body of the swamp is a losing system (discharges to groundwater). The time series data (see **Figure 6, Appendix A**) also shows the relative water level at GW18 consistently greater than GW14 (vertical hydraulic gradient downwards) over the monitored period.
- LTA The groundwater level in the LTA bore is consistently 0.3 m higher than the deeper UTAM/QA bore. Thus although there is an apparent driving head in the underlying LTA, this does not appear to have been transmitted into the UTAM/QA, given the head difference and observed \\aumel1fp001\projects\6055\6055006\500_DELIV\503_Hydrogeology Summary Report\60595006-ENV-RPT-002_Hydrogeology Summary Report_Rev4.docx Revision 4 - 06-Jun-2019 Prepared for - WIM Resource Pty Ltd - ABN: 59159389929

downward hydraulic gradient seen within the aquifer. This provides clear evidence that the Geera Clay, in this location at least, is acting as effective hydraulic barrier.

2.2.4 Connectivity between LTA and UTAM/QA

The potential for any hydraulic connectivity between the LTA (Renmark Group Aquifer) and the UTAM/QA (upper aquifer within the LPS) is the controlled by the permeability of the Geera Clay and hydraulic gradient between the overlying and underlying aquifers.

WIM's resource drilling, and the additional drilling undertaken during various groundwater investigations, show the Geera Clay is present across the entire Mine footprint and also the wider RL2014. It has been logged to be predominantly a high plasticity, silty-sandy, clay with a thickness typically greater than 40 m beneath the Mine, where it has been fully intersected.

It is noted that outside RL2014 (adjacent to Darlot Swamp) the Geera Clay thickness has been interpreted to be approximately 13 m. However, it is at this location that the head different between the two aquifers above and below is recorded to be in the order of +0.3m, with no evidence of the pressure head being transmitted across the unit.

Thus, where the Geera Clay is found to be the thinnest, there is strong evidence to show there is no material hydraulic connection between the LTA and UTAM/QA, and gives confidence that beneath the Mine footprint, where it is observed to be thicker sequence, a similar lack of hydraulic connection can be assumed.

2.3 Groundwater quality

The February 2019 groundwater bore installation development records are presented in **Table 2**, **Appendix B**, with laboratory results from a number of groundwater samples collected in March 2019 presented in **Appendix D**.

The groundwater sample results provide the following information on baseline conditions beneath the proposed Mine:

2.3.1 Salinity

UTAM / QA

Six (6) monitoring bores screen in the UTAM/QA were sampled:

- Bores GW14, GW18 and GW22, are located adjacent to Darlot and Dooen swamps, with salinity reported at 13,000 mg/L 7,280 mg/L and 6,890 mg/L respectively.
- Bores adjacent to Darlot Swamp (GW14 and GW18) are constructed as a shallow and deep pair within the water table UTAM /QA aquifer. The shallow screened bore GW18 indicates a fresher water quality (7,280 mg/L) as compared with GW14 which is screened at the base of the aquifer, where salinity is 13,000 mg/L. These results are consistent with the calculated downward vertical hydraulic gradients (refer Section 2.2.3) adjacent to Darlot swamp, suggesting that fresher water captured in the swamp infiltrates downward and outwards to the underlying aquifer.
- Bore GW22, adjacent to Dooen Swamp and screened at the base of the UTAM/QA, suggests a similar (relatively fresher) environment as GW18 and some level of dilution due to recharge from the adjacent swamp, as compared to background (field parameters in GW19).

Although not sampled for water quality in March 2019, post development of groundwater bore GW19, adjacent to Two Mile Creek (data presented in **Appendix C**), recorded an EC of 14,910 μ S/cm, equivalent to 9,691 mg/L TDS using the same conversion factor as the laboratory², noting that the bore is screened at the base of the UTAM/QA.

Samples from bores across the wider Mine footprint (GW05, GW21 and GW20) reported salinity ranging from 6,360 mg/L to 13,000 mg/L indicating that salinity is variable across the UTAM/QA and can be higher than anticipated. This compares with the publically available regional salinity mapping (as presented in GHD, 2018a) which indicates groundwater salinity (as TDS) within the UTAM/QA is in the order of 3,000 to 7,000 mg/L.

The variability in groundwater salinity observed in the UTAM/QA is likely a reflection of its heterogeneous nature, the proximity to recharge features (such as swamps/creeks) and the connectivity of higher permeability zones, such as the 'stringer' channels associated with higher energy depositions, to these recharge features.

LTA

No bores were sampled as part of the March 2019 groundwater monitoring event, however publically available regional salinity mapping (as presented in GHD, 2018a) indicates salinity in the LTA is in the order of 3,000 mg/L to 7,000 mg/L at the southern end of the Project area, increasing to 7,000 mg/L to 14,000 mg/L at the northern end of the Project area.

Bores screened in the LTA within and outside RL2014 (GW10, INV02 and INV03) were developed in April 2018 (GHD, 2018b) and field measurements taken. The field measurements show salinities of between 4,056 mg/L and 14,612 mg/L, which are consistent with regional mapping.

2.3.2 Major lons

Major ions were analysed for from samples collected during the March 2019 groundwater monitoring event. **Figure 10, Appendix A** compares the ionic composition of the water samples collected from each bore. All bores samples show a Sodium (Na) + Potassium (K) – Chloride (Cl) dominant water type. Sample GW20 has a slightly higher Sulfate (SO₄) concentration, whilst GW22 exhibits a slightly higher Na concentration.

² Salinity as mg/L TDS = Electrical Conductivity (μ S/cm) x 0.65

^{\\}aumel1fp001\projects\6055X\60595006\500_DELIV\503_Hydrogeology Summary Report\60595006-ENV-RPT-002_Hydrogeology Summary Report_Rev4.docx Revision 4 – 06-Jun-2019

4

All waters plot along the central right portion of the hydro-chemical facies diamond indicating the alkalies exceed alkalkine earth metals, which is common for recharge water originating from rainfall infiltration.

There does not appear to be any major differences between the hydro-chemical facies of bores GW14 and GW18 screened at the upper and lower portions of the UTAM/QA or between bores positioned adjacent to swamps and the bores positioned within the ore body.

3.1 Surface Water – Groundwater Interaction

3.1.1 Water Courses and Water Bodies

The surface topography, registered water courses and water bodies are presented in **Figure 2**, **Appendix A**, and include a number of artificial waterways within RL2014's boundary. This includes the Dooen Main Channel, Dooen East Channel, College Channel and the Jung West Channel. It is noted that the majority of these have been decommissioned, no longer in operation and/or are disconnected from the catchment since the commissioning of the Wimmera Mallee Pipeline (completed between 2006 and 2010).

The remaining key water bodies are discussed below:

3.1.2 Dooen Swamp

The Dooen Swamp has been reported to be a deep freshwater marsh (GHD, 2018) located adjacent and south west of RL2014, and approximately 2.0km from the Mine. In general, there is anecdotal evidence to suggest this swamp and Darlot Swamp have been modified through drainage and levelling since land development for agriculture during the 19th and 20th centuries.

The swamp is situated within 500 m (north) of the Wimmera River and is mapped as overlying Quaternary (Holocene) aged Unnamed Alluvium, consisting gravel, sand and silt. The swamp appears to have formed on the lithological boundary between the Quaternary Unnamed Alluvium and the adjacent Quaternary/Tertiary Shepparton Formation (fluvial and lacustrine sediments consisting of sands, gravels and clays).

Potential Groundwater Dependant Ecosystem (GDE) mapping undertaken by the Bureau of Meteorology (BoM) identify the swamp as having a low aquatic GDE potential. GHD (2018a) made comment that the wetland is ephemeral and is expected to be a losing surface water feature. The swamp is also classified by the BoM as having a high potential for supporting terrestrial GDEs.

Investigation works undertaken in 2019 have focused on assessing the potential groundwater connectivity to the swamp:

- Topographic survey:
 - Recent 1 m Lidar estimates the low point within Dooen Swamp is between 125 and 126 mAHD.
- Groundwater levels:
 - GW22 is installed approximately 250 m from the lowest surface point in the Dooen Swamp.
 - The LPS appears to have been eroded at GW22 and replaced with more recent Quaternary sediments associated with the surface drainage features.
 - Groundwater elevation at GW22 is reported at between 119.04 and 119.11 mAHD (March to May 2019), indicating that the water table is at least 5.9m below the swamp.

Overall the 2019 information shows the following in regards groundwater – surface water connectivity at Dooen Swamp:

- forms part of a historical river course feature that is likely to be (hydraulically) connected to the Wimmera River;
- not an aquatic GDE based on the observed depth to groundwater and the interpreted flow direction northwards, away from the swamp;
- groundwater salinity is marginally fresher beneath the swamp as compared to down flow path adding to the conceptual understanding that the swamp is likely a periodic recharge area for groundwater (i.e. limited to major flood events), and can be classified as a losing system;

GHD (2018a) noted that there is a high potential for terrestrial GDEs to be dependent on groundwater beneath or around the swamp. However, the measured depth to groundwater of 5.9m suggests

\\aumel1fp001\projects\6055X\60595006\500_DELIV\503_Hydrogeology Summary Report\60595006-ENV-RPT-002_Hydrogeology Summary Report_Rev4.docx Revision 4 – 06-Jun-2019 although there is potential for terrestrial GDEs, this would only be the case if there exists deep rooted (phreatophyte) type vegetation that requires more than the periodic flooding, and is tolerant of brackish water.

3.1.3 Darlot Swamp

The Darlot Swamp is located to the east and adjacent to RL2014 and approximately 1.9km from the Mine footprint. The swamp is located in the Yarriambiack Creek and Two Mile Creek floodplain.

The surface geology underlying the swamp is mapped largely as Quaternary (Holocene) aged fluvial gravel, sand and silt, and to the north bounds Quaternary (Pleistocene) aged Shepparton Formation consisting fluvial silt, sand and minor gravels (Geology is shown on **Figure 1, Appendix A**).

The swamp appears to be hydraulically connected to the Yarriambiack Creek and therefore likely receives flows when distributed from the Wimmera River.

Flows reaching Darlot Swamp appear to then return, via Two Mile Creek (southward), back into the Wimmera River (Water Technology, 2015). GHD (2018a) noted that Darlot Swamp is an ephemeral, freshwater marsh, expected to be a losing surface water feature, with a low potential to be an aquatic GDE. The assumption is supported by evidence that Yarriambiack Creek is largely dry for most periods, with exceptions after prolonged rainfall or after receiving flows from the Wimmera River (Water Technology, 2015).

Investigation works undertaken in 2019 have focused on assessing the potential groundwater connectivity to the swamp:

- Topographic survey:
 - Recent 1 m Lidar estimates the low point within Darlot Swamp is between 132 and 133 mAHD.
- Groundwater levels:
 - GW18 drilled adjacent to swamp indicate that the entire thickness of Loxton Parilla Sands has been removed and replaced with more recent Quaternary (Alluvium) sediments adjacent at this location; and
 - GW14 and GW18 are located approximately 330 m of the swamp, where the water table is observed within the Quaternary Alluvium at 125.8 mAHD (based on March to May 2019 observations).

Overall the 2019 information shows the following in regards groundwater – surface water connectivity at Darlot Swamp:

- lithology beneath the swamp is of the QA aquifer;
- not an aquatic GDE based on the observed depth to groundwater of 6.2m below the lowest point of swamp's surface;
- groundwater flow is northwards, away from the swamp and downwards within the shallow and deep portions of UTAM/QA bores (GW18 and GW14 respectively); and
- groundwater salinity measurements beneath the swamp in the UTAM/QA bores increases from 7,280 mg/L to 13,000 mg/L, which suggest the swamp is a recharge feature.

GHD (2018a) noted that Darlot Swamp is unlikely to support terrestrial GDEs, as per the national GDE assessment. The 2019 information suggests a potential for terrestrial GDEs, but as with Dooen Swamp, this would only be the case if there exists deep rooted (phreatophyte) type vegetation that requires more than the periodic flooding, and is tolerant of brackish water.

3.1.4 Yarriambiack Creek and Two Mile Creek

Yarriambiack Creek is approximately 2.4 km from the eastern boundary of RL2014, flows generally north and drains into Lake Coorong, northeast of Hopetown. The creek is a distributary of the Wimmera River and leaves the Wimmera near Drung Drung, approximately 20 km east of Horsham.

Creek flow is intermittent and only significant rainfall events occurring within the catchment will generate flows. However, it is also noted that creek flow depends almost entirely on the level of the Wimmera River which distributes flow into the creek during certain periods. There are a number of weirs built along the creek to hold water.

During high flows, the majority of flow distribution to Yarriambiack Creek (from the Wimmera River) returns to the Wimmera River via Two Mile Creek (and subsequently through Darlot Swamp). Approximately 30% of flow distributed from the Wimmera River continues northwards along Yarriambiack Creek (Water Technologies, 2015).

The creek is subject to flooding, notable flood events are recorded for 1909, 1981, 1983 and most recently in September 2010 and January 2011 after not flowing for most of 1995 – 2010.

Lidar data provided by WIM is presented in **Figure 2**, **Appendix A**. Lidar along Yarriambiack Creek indicates a very subtle fall along each of the drainage lines:

- At Wimmera Highway, 1,500 m North of Darlot Swamp The lowest observed LIDAR point is 131 mAHD;
- East of Jung Tip Road, 2,700 m North of Darlot Swamp, the lowest observed LIDAR point is 129 mAHD; and
- At Green Hills Road, ~5,000 m North of Darlot Swamp, the lowest observed LIDAR point is 128 mAHD.

Mapped groundwater table elevation contours within RL2014, west of these points infer the water table is between 125 and 115 mAHD, groundwater contours show a north – northwest flow direction, away from Yarriambiack Creek.

Similarly to Yarriambiack Creek, the topography fall along Two Mile Creek appears to be subtle:

- South (300 m) of GW19, the lowest observed LIDAR point is 131 mAHD; and
- Where Two Mile Creek reaches the Wimmera River, the lowest observed LIDAR point is 128 mAHD.

Adjacent to Two Mile Creek at GW19, depth to groundwater is less than 7 m below ground level, the groundwater elevation is around 126.3 mAHD (observed March to May 2019), Groundwater gradients infer flow direction is north, away from Two Mile Creek (and subsequently away from the Wimmera River). Depth to groundwater may become shallower in closer proximity to the creek, becoming readily accessible to terrestrial GDEs. Salinity estimates (from post development EC measurements) do not appear to suggest any freshening of the aquifer at GW19.

4.0 Conclusions

The factual outcomes from the 2019 field investigations are as follows:

- The upper aquifer (referred to as the UTAM/QA) beneath the Mine is brackish (salinity generally 6,000 to 13,000 mg/L TDS) with limited users in the vicinity of the mine plan area (only two registered stock and domestic bores within a 5 km radius).
- Groundwater within the upper aquifer shows a general increase in salinity down flow path (northwards), away from the surface drainage features present south of the proposed Mine.
- There is little change in hydro-geochemistry between up-gradient bores (south), those adjacent to surface drainage features, bores screened within the mineralised zone and down gradient outside of the mineralised zone (north).
- Geera Clay is found to consist of a high plasticity clay unit beneath entire Mine site, with an
 observed head difference between the overlying (UTAM) and underlying (LTA) aquifers where
 monitored.
- The depth to groundwater beneath the lowest points of Darlot and Dooen Swamps is greater than 5 metres (measured in March 2019 at 5.9 and 6.2m respectively).
- Downward vertical gradient immediately adjacent to swamps.

The implications of this updated factual information on the potential groundwater risks are as follows:

- The ephemeral swamps (Dooen and Darlot) are losing systems, whereby they recharge the underlying aquifer whenever they fill with surface water flows.
- The depth to groundwater, vertical hydraulic gradient and groundwater salinity profile indicates that within Dooen Swamp and Darlot Swamp there is:
 - no potential for aquatic GDEs;
 - potential for terrestrial GDEs, but only if there exists deep rooted (phreatophyte) type vegetation that requires more than the periodic flooding, and is tolerant to brackish water.
- The mining of the mineral sands within the project area will require dewatering the upper aquifer (UTAM/QA) by less than 10 metres. The extent of the resultant cone of depression will be limited by the relatively low permeability and temporal period of dewatering.
- Any tailings disposal into the mining voids will result in seepage of water entering the upper aquifer system, and will result in some level of mounding and changes to groundwater quality. The brackish nature and limited users of the upper aquifer in the Project area mean the consequences are likely to be minor.
- Limited risks to the underlying Renmark Group aquifer (LTA) from either dewatering or mounding in the upper aquifer (UTAM) given the nature and occurrence of the mapped Geera Clay aquitard.

5.0 Limitations

AECOM Australia Pty Limited (AECOM) has prepared this report in accordance with the usual care and thoroughness of the consulting profession for the use of WIM Resource Pty Limited and only those third parties who have been authorised in writing by AECOM to rely on this Report.

It is based on generally accepted practices and standards at the time it was prepared. No other warranty, expressed or implied, is made as to the professional advice included in this Report.

It is prepared in accordance with the scope of work and for the purpose outlined in the variation (email) request dated 20 May 2019, under the Hydrology – Critical Review contract dated 18 December 2018

Where this Report indicates that information has been provided to AECOM by third parties, AECOM has made no independent verification of this information except as expressly stated in the Report. AECOM assumes no liability for any inaccuracies in or omissions to that information.

This Report was prepared between 20 May 2019 and 28 May 2019 and is based on the information reviewed at the time of preparation. AECOM disclaims responsibility for any changes that may have occurred after this time.

This Report should be read in full. No responsibility is accepted for use of any part of this report in any other context or for any other purpose or by third parties. This Report does not purport to give legal advice. Legal advice can only be given by qualified legal practitioners.

Except as required by law, no third party may use or rely on this Report unless otherwise agreed by AECOM in writing. Where such agreement is provided, AECOM will provide a letter of reliance to the agreed third party in the form required by AECOM.

To the extent permitted by law, AECOM expressly disclaims and excludes liability for any loss, damage, cost or expenses suffered by any third party relating to or resulting from the use of, or reliance on, any information contained in this Report. AECOM does not admit that any action, liability or claim may exist or be available to any third party.

Except as specifically stated in this section, AECOM does not authorise the use of this Report by any third party.

It is the responsibility of third parties to independently make inquiries or seek advice in relation to their particular requirements and proposed use of the site.

Any estimates of potential costs which have been provided are presented as estimates only as at the date of the Report. Any cost estimates that have been provided may therefore vary from actual costs at the time of expenditure.

6.0 References

AECOM 2019, Hydrogeological Gap Analysis – Avonbank Heavy Mineral Sands Project. Letter report no# 60595006-ENV-LTR-001, prepared for WIM Resource Pty Ltd, Melbourne Victoria, May 2019

AECOM, 2019. Bore Completion Report. Report no# 60595006-ENV-RPT-001, prepared for WIM Resource Pty Ltd, Melbourne Victoria, May 2019.

ATCW, 2017. "*Report on Geotechnical Drilling Program, Preliminary Assessment of Pit Slopes, Trafficability and Excavabaility*." Report no: 115138.01, prepared by ATC Williams, Melbourne, June 2017.

DSE, 2012. "*Victorian Aquifer Framework Updates for Seamless Mapping of Aquifer Surfaces.*" Report no: 31/27999/207086, prepared by GHD Pty Ltd for the Victorian Government Department of Sustainability and Environment, Melbourne, May 2012.

EPA, 2000. "*Groundwater Sampling Guidelines*." Publication 669, prepared by the Victorian Government Environmental Protection Agency, Southbank, April 2000.

GHD 2018a. "Avonbank HMS Project Desktop Hydrogeological Assessment." prepared by GHD, August 2018.

GHD 2018b. "Avonbank HMS project Groundwater monitoring bore and aquifer testing completion report." prepared by GHD, August 2018.

GHD 2018c. "Groundwater Modelling Results." prepared by GHD, October 2018

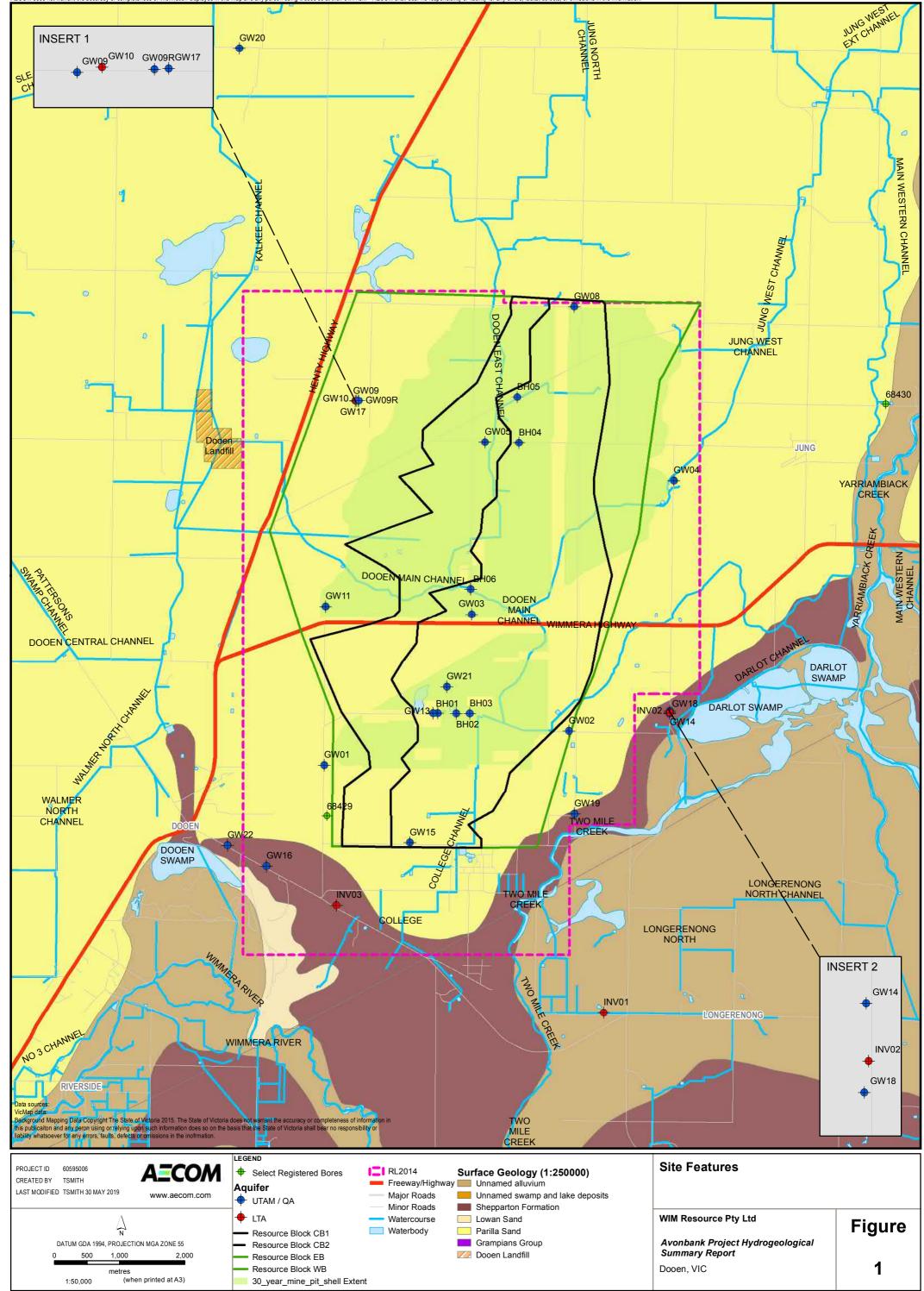
Water Technology 2015. "*Warracknabeal and Brim Flood Investigation – Hydrology and Hydraulics*." Report R01 (reference 3532-01) prepared for Wimmera CMA, Notting Hill, Victoria.

URS, 2010 "Grampians West Groundwater Resource Appraisal." Report 43325977/1/4 prepared for Grampians Wimmera Mallee Water, June 2019

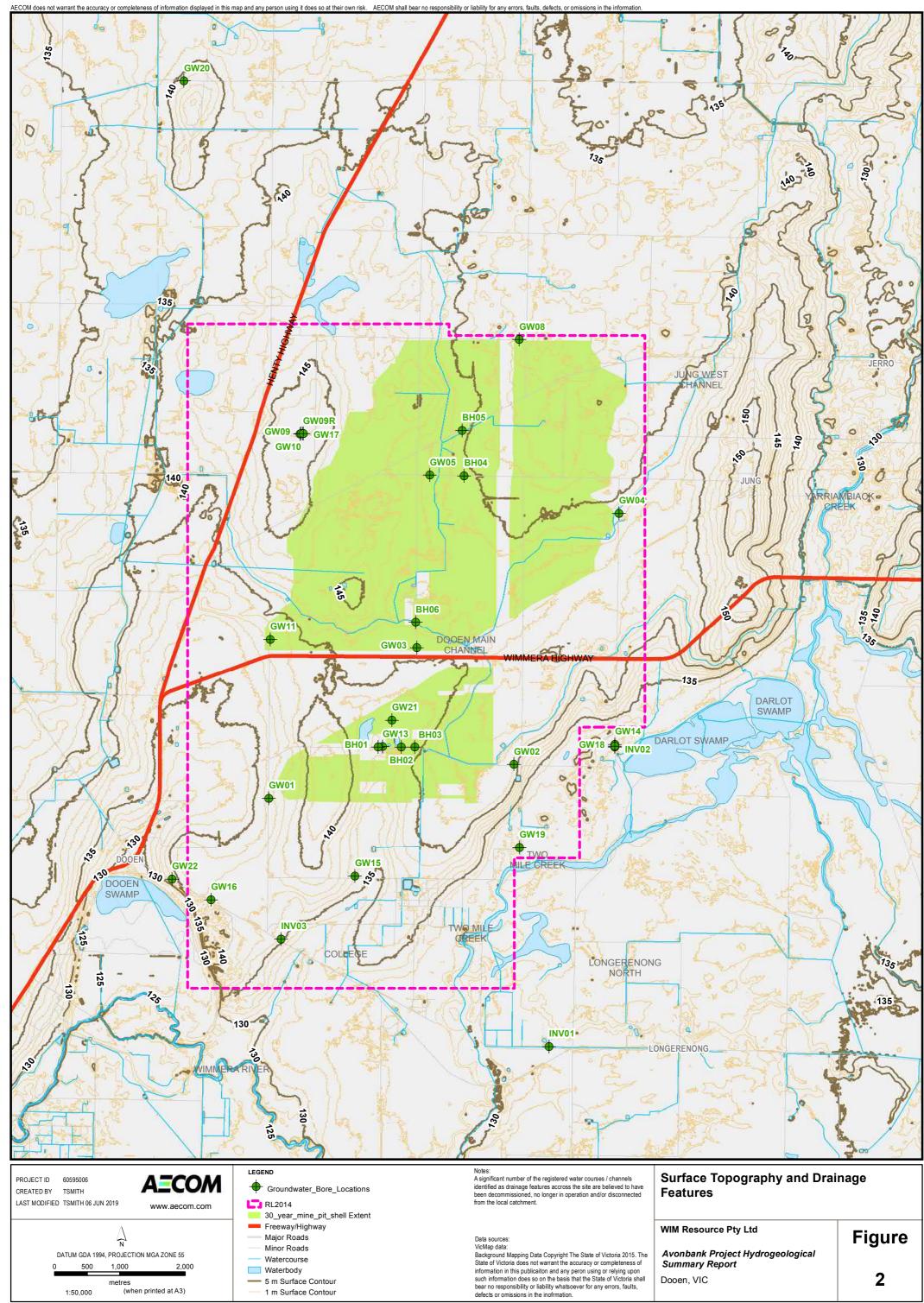
Appendix A

Figures

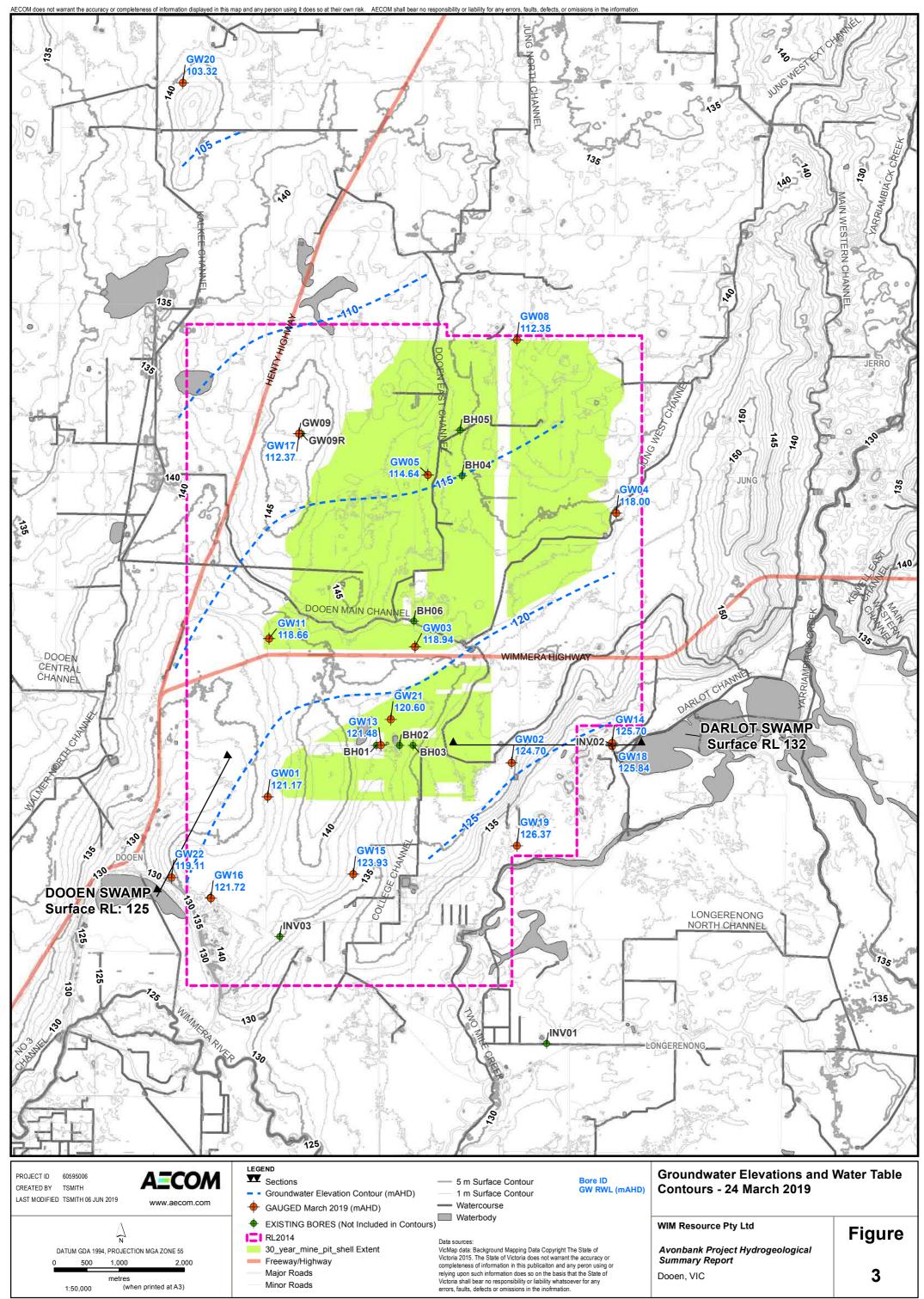
Appendix A Figures



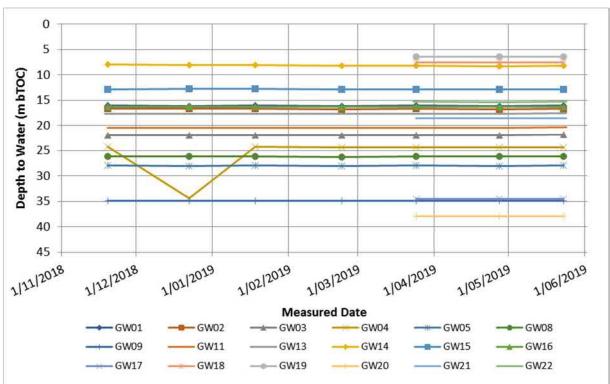
Map Document: (\\aumel1fp001\projects\605X\60595006\900_CAD_GIS\920_GIS\MXD\03 Hydro Summary Report\60595006_F1_SiteFeatures.mxd)



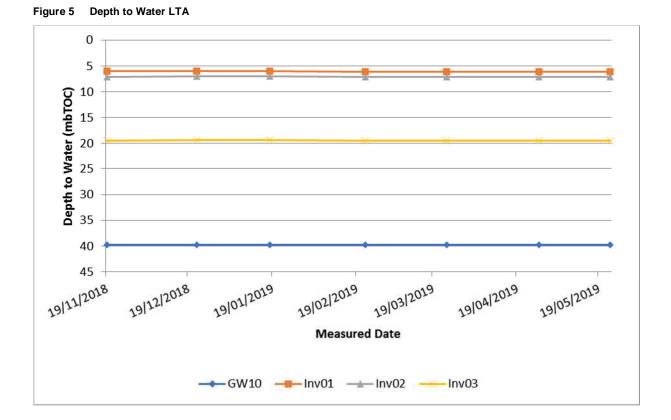
Map Document: (\\aumel1fp001\projects\6057\60595006\900_CAD_GIS\920_GIS\MXDI03 Hydro Summary Report\60595006_F2_Topography and Drainage.mxd)



Map Document: (\\aumel1fp001\projects\605X\60595006\900_CAD_GIS\920_GIS\MXD\03 Hydro Summary Report\60595006_F3_GWContours.mxd)

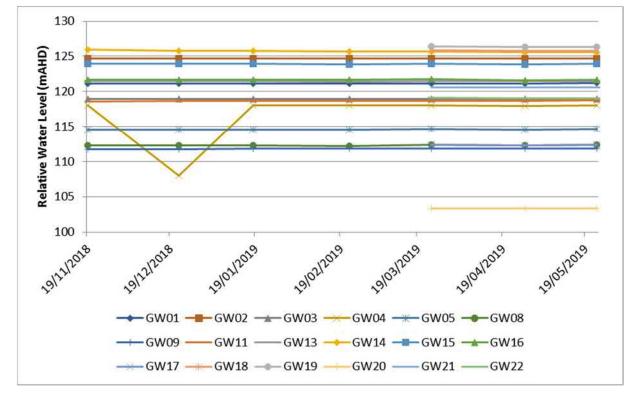


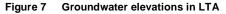


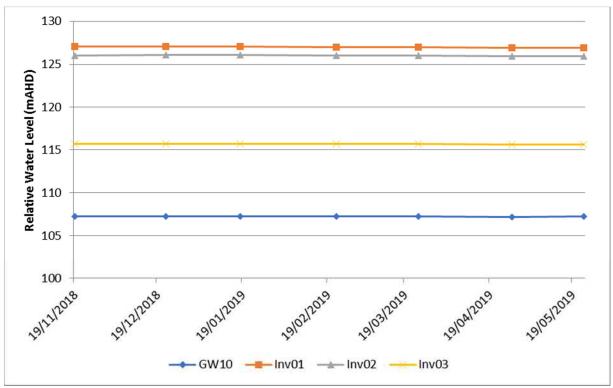


\\aumel1fp001\projects\6055X\60595006\500_DELIV\503_Hydrogeology Summary Report\60595006-ENV-RPT-002_Hydrogeology Summary Report_Rev4.docx Revision 4 – 06-Jun-2019 Prepared for – WIM Resource Pty Ltd – ABN: 59159389929

Figure 6 Groundwater elevations in UTAM / QA







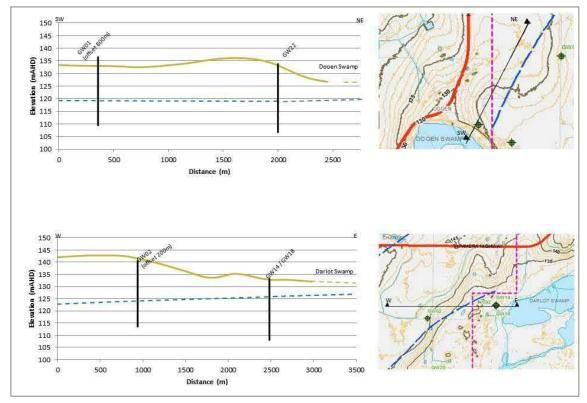
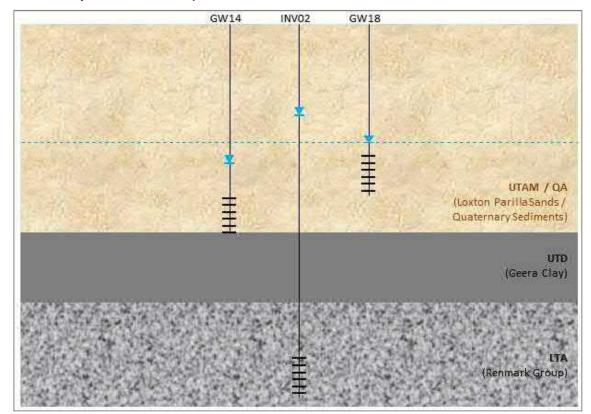


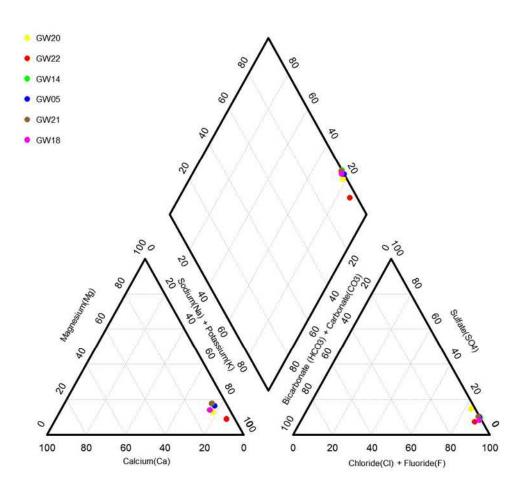
Figure 8 Cross Section Schematics of surface topography and water table elevations at Dooen Swamp and Darlot Swamp interpolating depth to water below ground surface

Figure 9 Indicatives schematic of water levels and differences in hydraulic heads between UTAM/QA and LTA, adjacent to Darlot Swamp



\\aumel1fp001\projects\6055X\60595006\500_DELIV\503_Hydrogeology Summary Report\60595006-ENV-RPT-002_Hydrogeology Summary Report_Rev4.docx Revision 4 – 06-Jun-2019 Prepared for – WIM Resource Pty Ltd – ABN: 59159389929

Figure 10 Piper plot of March 2019 major ion analysis



Appendix **B**

Tables

Appendix B Tables



Table 1 - 2019 Groundawter Bore Monitoring Locations

Location	Location ID	Installation Date	Easting (m)	Northing (m)	Surface Elevation (m AHD)	PVC Reference	Point (1()(C)	Steel Casing Height (m agl)	Casing Diameter (mm)	Drilled Depth (m bgl)	Screened From (m bgl)	Screened To (m bgl)
Drovers Rd	GW17	22/02/2019	614727.05	5948496.53	146.19	146.85	0.66	0.73	50	45	36.0	42.0
Drung-Jung Rd	GW18	20/02/2019	619541.33	5943688.30	132.82	133.40	0.59	0.69	50	18	8.0	14.0
Tuckers Rd	GW19	23/02/2019	618076.95	5942154.74	132.05	132.78	0.73	0.85	50	36	23.0	29.0
Banyena Rd	GW20	21/02/2019	612941.10	5953898.25	140.73	141.24	0.51	0.62	50	46	35.0	41.0
Test Pit Crest	GW21	26/02/2019	616136.46	5944104.59	138.60	139.16	0.56	0.68	50	31	21.0	27.0
Longerong Rd	GW22	18/02/2019	612768.48	5941667.44	133.74	134.41	0.67	0.78	50	30	22.0	28.0

Surveyed 26 March 2019



Table 2 - 2019 Groundwater Bore Development Results

	Development Date(s)	Pre Develop SWL (m btoc)	Post Develop SWL (m btoc)	Volume Removed (L)	pH (p⊦	I units)	Electrical Conductivity (µS/cm)		Post DevelopmentComment
Location ID	Date(S)			Kellioved (L)	Pre	Post	Pre	Post	
GW17	24 & 26/02/2019	34.06	33.85	60	10.54	8.37	1,954	12,555	Dark Brown, fines in sample
GW18	24/02/2019	7.56	8.66	330	12	8.6	2,333	10,850	Clear, non turbid
GW19	24/02/2019	6.30	6.53	500	7.79	12.75	2,953	14,910	Clear, non turbid
GW20	25 & 26/02/2019	37.85	37.89	80	9.31	8.3	5,275	8,145	Brown-grey, distinctly fresher than other bores.
GW21	26/02/2019	17.60	17.8	300	10.67	8.57	2,127	12,580	Slightly cloudy
GW22	24 & 26/02/2019	4.92	14.54	95	11.44	8.19	32,775	10,164	Brown-yellow, turbid

mbtoc metres below top of casing

Table 3 - 2018/2019 Manual Groundwater Level Gauging Data

		C	Depth To Wate	er (m below T	op of Casing)	
Bore ID	19/11/2018						23/05/2019
Upper Te	ertiary Aqifer (N	/larine) / Quat	ernary Aquifer	[.] - Loxton Pari	illa Sands		
GW01	16.12	16.14	16.12	16.16	16.11	16.17	16.1
GW02	16.72	16.74	16.73	16.78	16.74	16.79	16.74
GW03	22.01	22.02	21.97	22	21.98	21.99	21.94
GW04	24.32	34.35	24.32	24.39	24.38	24.41	24.37
GW05	27.99	28.04	27.99	28.06	27.94	28.02	27.95
GW08	26.2	26.24	26.23	26.25	26.13	26.21	26.14
GW09	34.91	34.91	34.9	34.9	34.87	34.89	34.89
GW11	20.54	20.52	20.51	20.52	20.49	20.49	20.41
GW13	17.68	17.68	17.67	17.7	17.66	17.68	17.64
GW14	7.92	8.14	8.13	8.19	8.19	8.29	8.26
GW15	12.85	12.8	12.81	12.88	12.85	12.91	12.87
GW16	16.28	16.3	16.28	16.33	16.26	16.36	16.31
GW17	-	-	-	-	34.48	34.53	34.47
GW18	-	-	-	-	7.56	7.59	7.6
GW19	-	-	-	-	6.41	6.48	6.44
GW20	-	-	-	-	37.92	37.92	37.91
GW21	-	-	-	-	18.56	18.6	18.56
GW22	-	-	-	-	15.3	15.37	15.35
Lower Te	rtiary Aquifer	- Renmark Gr	oup				
GW10	39.79	39.79	39.77	39.8	39.77	39.82	39.78
Inv01	6.02	6.02	6.04	6.11	6.14	6.18	6.15
Inv02	7.09	7.04	7.08	7.13	7.15	7.19	7.2
Inv03	19.42	19.41	19.4	19.43	19.43	19.47	19.46

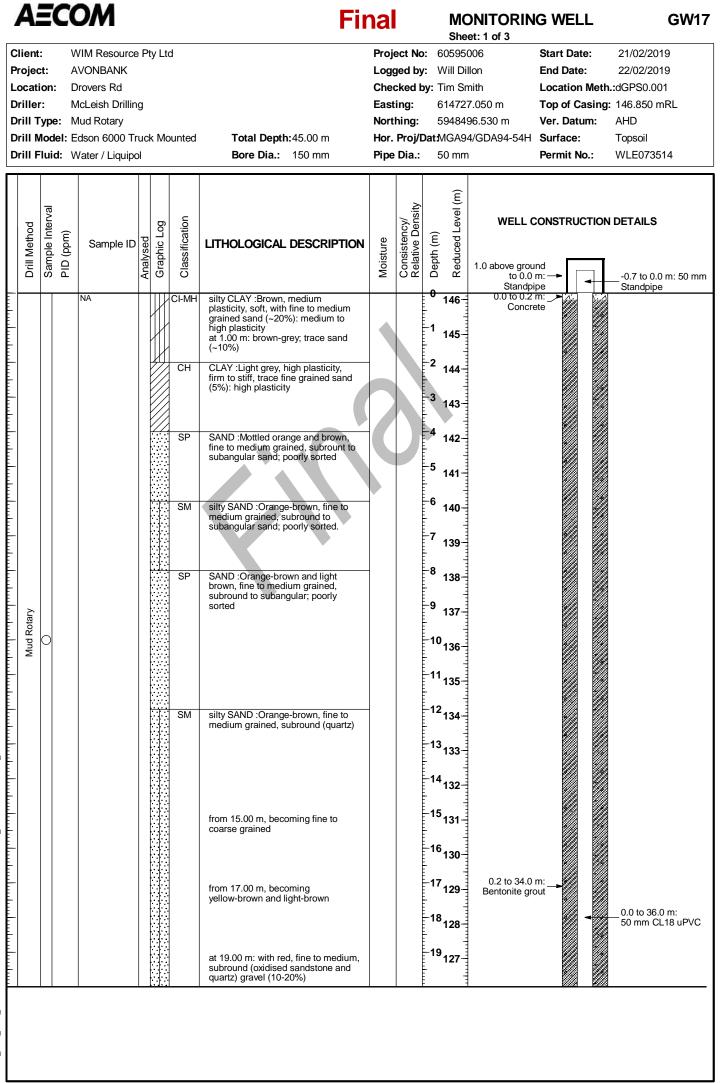
Table 4 - 2018/2019 Relative Water Levels

		Relativ	ve Water Lev	els (m Austra	alian Height D	atum)	
Bore ID	19/11/2018	22/12/2018	18/01/2019	22/02/2019	24/03/2019	27/04/2019	23/05/2019
Upper Ter	rtiary Aqifer (M	larine) / Quate	ernary Aquifer	⁻ - Loxton Pari	illa Sands		
GW01	121.16	121.14	121.16	121.12	121.17	121.11	121.18
GW02	124.72	124.7	124.71	124.66	124.7	124.65	124.7
GW03	118.91	118.9	118.95	118.92	118.94	118.93	118.98
GW04	118.06	108.03	118.06	117.99	118	117.97	118.01
GW05	114.59	114.54	114.59	114.52	114.64	114.56	114.63
GW08	112.28	112.24	112.25	112.23	112.35	112.27	112.34
GW09	111.78	111.78	111.79	111.79	111.82	111.8	111.8
GW11	118.61	118.63	118.64	118.63	118.66	118.66	118.74
GW13	121.46	121.46	121.47	121.44	121.48	121.46	121.5
GW14	125.97	125.75	125.76	125.7	125.7	125.6	125.63
GW15	123.93	123.98	123.97	123.9	123.93	123.87	123.91
GW16	121.7	121.68	121.7	121.65	121.72	121.62	121.67
GW17	-	-	-	-	112.368	112.318	112.378
GW18	-	-	-	-	125.844	125.814	125.804
GW19	-	-	-	-	126.369	126.299	126.339
GW20	-	-	-	-	103.322	103.322	103.332
GW21	-	-	-	-	120.596	120.556	120.596
GW22	-	-	-	-	119.113	119.043	119.063
Lower Ter	rtiary Aquifer -	Renmark Gro	oup				
GW10	107.24	107.24	107.26	107.23	107.26	107.21	107.25
Inv01	127.07	127.07	127.05	126.98	126.95	126.91	126.94
Inv02	126.04	126.09	126.05	126	125.98	125.94	125.93
Inv03	115.69	115.7	115.71	115.68	115.68	115.64	115.65

Appendix C

Bore Logs

Appendix C 2019Bore Completion Report



4			VIM Resource	> P	hv I t	d		na		She c: 60595	eet: 2 of 3	Start Date:	21/02/2019
ojec			VONBANK			u		-		y: Will Di		End Date:	22/02/2019
cati	ion	: C	Provers Rd					Che	cked l	by: Tim Sr	mith	Location Met	h.:dGPS0.001
ille			IcLeish Drillir	ŋg				East	•		7.050 m		g: 146.850 mRL
			lud Rotary dson 6000 Ti	ruc	k Mr	ounted	Total Depth:45.00 m		hing: Proi/		96.530 m 4/GDA94-54H	Ver. Datum: Surface:	AHD Topsoil
			Vater / Liquip			Junieu	Bore Dia.: 150 mm		Dia.:			Permit No.:	WLE073514
Drill Method	Sample Interval	PID (mpm)	Sample ID	Analysed	Graphic Log	Classification	LITHOLOGICAL DESCRIPTION	Moisture	Consistency/ Relative Density	Depth (m) Reduced Level (m)	WELL	CONSTRUCTIO	N DETAILS
			NA			SM	silty SAND :Orange-brown, fine to medium grained, subround (quartz)			²⁰ 126			
							at 21.00 m: absence of gravel			⁻²¹ 125-			
										E 3			
							from 22.00 m, becoming fine to coarse			⁻²² 124-			
					.,	SP-SC	clayey SAND :Pale grey, fine to coarse grained, subround with clay (~10%)			⁻²³ 123-			
					/,				\cup	⁻²⁴ 122-			
							at 25.00 m: clay matrix grades to orange and pale grey			-25 ₁₂₁ -			
					/			× ·		⁻²⁶ 120-			
					/		at 27.00 m: abesnce of clay, trace subround (quartz) gravel (<5%)			⁻²⁷ 119			
					/					⁻²⁸ 118			
otary					//		at 29.00 m: with orange, low plasticity clay (<10%)			⁻²⁹ 117-			
Mud Rotary	0				/		at 30.00 m: absence of clay			- ³⁰ 116-			
					/					⁻³¹ 115-			
					/					- ³² 114-			
					/					⁻³³ 113-			
						CL	sandy CLAY :Pale grey and red, low plasticity; with fine to medium grained, subround to subangular sand.: low plasticity from 24 00 m, becoming light brown			-34 112-	Standing wa level at 33.8 26/02/20	5 m — 🗕 🌌 📓	
							from 34.00 m, becoming light-brown from 35.00 m, becoming red, trace			- ³⁵ 111-	Bentonite pe) m: 📕	
							fine to coarse, angular sand			E i			
						CL	sandy CLAY :Dark grey, medium to high plasticity, firm to stiff ; with fine to medium grained (quartz) sand:			- ³⁶ 110-			
						SW	Low plasticity SAND :Mottled pale brown, grey, red, yellow, medium to coarse	1		⁻³⁷ 109-			
						SM	graiend, well sorted (quartz) silty SAND :Pale brown, fine to medium grained, subround (quartz)			⁻³⁸ 108-	35.0 to 42.0 8/16" Filter sa		36.0 to 42.0 m:
						СН	CLAY :Dark grey, medium to hgh plasticity, firm to stiff; with fine to medium grained sand (quartz): high			⁻³⁹ 107-			50 mm CL18 uPV0 0.4mm machine slotted screen

AΞC	:OM		Fi	nal	MONITORI Sheet: 3 of 3	NG WELL	GW17
Drill Mode	WIM Resource I AVONBANK Drovers Rd McLeish Drilling Mud Rotary I: Edson 6000 Tru Water / Liquipol	l Ick Moun	ed Total Depth: 45.00 m Bore Dia.: 150 mm	Logged by: Checked by Easting: Northing:	: 60595006 : Will Dillon y: Tim Smith 614727.050 m 5948496.530 m attMGA94/GDA94-54 50 mm	Ver. Datum:	21/02/2019 22/02/2019 a.:dGPS0.001 : 146.850 mRL AHD Topsoil WLE073514
Drill Method Sample Interval	E Sample ID	Analysed Graphic Log	LITHOLOGICAL DESCRIPTION	Moisture Consistency/ Relative Density	Depth (m) Reduced L	CONSTRUCTION	I DETAILS
Mud Rotary	NA		M \plasticity :Dark grey, highly indurated band: fine to medium grained sandy CLAY :Dark grey to black, medium to high plasticity, sand is fine to medium grained: low plasticity CLAY :Dark grey, medium to high plasticity, stiff; with fine to medium grained sand (~20%) (fragments of organic white shells): high plasticity		-43 103 - 43.0 to 45. Filter	seal	

Drill Mo	n: D N pe: M pdel: E	/IM Resource VONBANK Irung-Jung Rd IcLeish Drilling Iud Rotary dson 6000 Tri /ater / Liquipo	l g uck M		Total Depth:18.00 m Bore Dia.: 150 mm	Logo Cheo East Nort Hor.	ged by cked b ing: hing:	59436	illon mith 1.330 m 88.300 m 14/GDA94-54H	Ver. Datum:	19/02/2019 20/02/2019 a.:dGPS0.001 g: 9999.000 mRL AHD Topsoil WLE073514
Drill Method Samola Interval	PID (ppm)	Sample ID	Analysed Graphic Log	Classification	LITHOLOGICAL DESCRIPTION	Moisture	Consistency/ Relative Density	 Depth (m) Reduced Level (m) 	1.0 above grour to 0.0 r Standpip	m:→ →	N DETAILS 0.8 to 0.0 m: 50 mm Standpipe
				CI SC CL SW SC	silty CLAY :Dark grey, medium to high plasticity, firm; trace fine to coarse grained subround sand (<5%): medium plasticity from 1.00 m, becoming brown-grey from 2.00 m, becoming orange-brown sandy CLAY :Light brown, low to medium plasticity, firm; fine to medium grained sand (30%) silty CLAY :Pale brown, medium to high plasticity; trace fine grained sand (<10%): low plasticity SAND :Pale grey mottled brown, fine to coarse grained, well graded subround sand, clays are medium to high plasticity (-20%) at 11.00 m: Grey and orange-brown SAND :Orange-brown and pale grey, fine to coarse grained, well sorted and subround (quartz)			0 1 132- 2 131- 3 130- 4 129- 5 128- 6 127- 7 126- 8 125- 9 124- 10 123- 11 122- 12 121- 13 120- 14 119- 14 119- 15 118- 16 117- 17 116- 18 115- 19 114- 1013- 113-	7.0 to 14.0 r 8/16" Filter sar 14.0 to 18.0 r Bentonite pell se	n: er m: er h: h: h: h: h: h: h: h: h: h:	0.0 to 8.0 m: 50 mm CL18 uPVC 8.0 to 14.0 m: 50 mm CL18 uPVC, 0.4mm machine slotted screen

	WIM Resource AVONBANK Tuckers Rd McLeish Drilling Mud Rotary Edson 6000 Tru	9		Total Depth:36.00 m	Logo Cheo East Nort	hing:	: Wi y: Tin 618 594	ll Dill n Sm 8076 4215	lon nith 6.950 m	Ver. Datum	2 Meth.:d sing: 8 n: A	2/02/2019 3/02/2019 GPS0.001 888.000 mRL HD opsoil
rill Fluid:	Water / Liquipol			Bore Dia.: 150 mm	Pipe	Dia.:	50	mm		Permit No.		/LE073514
Drill Method Sample Interval	Sample ID	Analysed Graphic Log	Classification	LITHOLOGICAL DESCRIPTION	Moisture	Consistency/ Relative Density	_	Reduced Level (m)	1.0 above grour to 0.0 r Standpip	n:→ De		ETAILS 0.8 to 0.0 m: 50 m Standpipe
Mud Rotary			CL CL CL CL CL CL CL CL	silty CLAY :Grey, low to medium plasticity, soft to firm; trace fine sand (5%): low plasticity CLAY :Brown-grey, high plasticity, stiff: high plasticity silty CLAY :Yellow-brown and brown-grey, medium plasticity, firm, with fine grained sand (10%): low plasticity from 4.00 m, becoming orange-brown and grey-brown (streaky) from 5.00 m, becoming mottled yellow-brown and grey, with fine to coarse subangular sand (10-20%) (quartz) SAND :Orange-brown, fine to coarse grained, subround (quartz) at 7.00 m: grey-brown CLAY :Brown-grey, medium to high plasticity, firm to stiff; with fine to coarse grained subround sand (20%): high plasticity sandy CLAY :Brown-grey, low to medium plasticity, firm; fine to coarse grained subround sand: low plasticity clayey SAND :Brown-red, fine to coarse grained, subround to subangular sand; trace fine subangular to subround gravel (<5%) (quartz, oxidised sandstone) sandy CLAY :Brown, low to medium plasticity, firm to stiff; fine to medium grained, subround to subangular sand (quartz and sandstone): trace fine gravel (<5%): low plasticity silty SAND :Light-brown and orange-brown, fine to medium grained, subround to subangular (quartz); trace fine gravel (<5%) (quartz) at 14.00 m: red-orange, sand content is increasing			-1 1; - -2 1; -3 1; -	30 29 28 27 26 27 26 27 26 27 26 27 26 27 26 27 20 19 19 110 110 1111 11111111111111111	0.0 to 0.3 f Concre	er m 9		0.0 to 23.0 m: 50 mm CL18 uPVC

d erval	4. SP	LITHOLOGIC SM silty SAND :Lig orange-brown, grained, subrou (quartz and oxid P-SM gravelly SAND orange-brown, grained sand w subround to sul gravel (up to 8n (10-20%) SM silty SAND :Lig orange-brown, grained, subrou composition of the subrau orange-brown, grained, subrou (10-20%) SM silty SAND :Lig orange-brown, grained, subrou	fine to medium and to subangular dised sandstone) :Light-brown and fine to coarse ith fine to medium bangular (quartz) nm); with silth ht-brown and fine to medium and to subangular; ngular (quartz) gravel :Light-brown and fine to coarse.		Consistency/ Relative Density	50 mm (iii) Iava J peonpe (iii) Iava J peonpe 20112 - 21111 - -22110 - -23109 - -24108 - -25107 - -26106 -		et	23.0 to 29.0 m:
	4. SP	 SM silty SAND :Ligi orange-brown, grained, subrou (quartz and oxid orange-brown, grained sand w subround to sul gravel (up to 8r (10-20%) SM silty SAND :Ligi orange-brown, grained, subrou frace fine subar (5%) gravelly SAND orange-brown, grained sand; fine subar (5%) gravelly SAND orange-brown, gravelly SAND orange-brown	ht-brown and fine to medium and to subangular dised sandstone) :Light-brown and fine to coarse ith fine to medium bangular (quartz) nm); with silth ht-brown and fine to medium and to subangular; ngular (quartz) gravel :Light-brown and fine to coarse.	Moisture		-20112- -21111- -22110- -23109- -24108- -25107-	21.0 to 22.0 n Bentonite pello Sec 22.0 to 29.0 n	n: et	23.0 to 29.0 m:
Mud Rotary	6. SP 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.	 oránge-brown, grained, subrou (quartz and oxid) SM gravelly SAND orange-brown, grained sand w subround to sul gravel (up to 8n (10-20%) SM silty SAND :Lig orange-brown, grained, subrou (5%) gravelly SAND SM gravelly SAND Gravelly SAND GM gravelly SAND 	fine to medium and to subangular dised sandstone) :Light-brown and fine to coarse ith fine to medium bangular (quartz) nm); with silth ht-brown and fine to medium and to subangular; ngular (quartz) gravel :Light-brown and fine to coarse.			-21111- -22110- -23109- -24108- -25107-	Bentonite pello set	et	
Mud Rotary	2 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	orange-brown, grained sand w subround to sul gravel (up to 8n (10-20%) SM silty SAND :Lig orange-brown, grained, subrou trace fine subar (5%) gravelly SAND orange-brown, SM grained sand; fi	fine to coarse ith fine to medium bangular (quartz) nm); with silth ht-brown and fine to medium ind to subangular; ngular (quartz) gravel :Light-brown and fine to coarse			-23109 -24108 -25107-	22.0 to 29.0 n 8/16" Filter san		
Mud Rotary	•SP •	orange-brown, grained, subrou trace fine subar (5%) gravelly SAND orange-brown, SM grained sand; fi	fine to medium and to subangular; ngular (quartz) gravel :Light-brown and fine to coarse.	Г			22.0 to 29.0 n 8/16" Filter san	n:	
Mud Rotary	<u>a</u> S	orange-brown, M grained sand; fi	fine to coarse			20100			50 mm CL18 uPVC 0.4mm machine slotted screen
		grained, subrou (quartz) gravel fines (10-20%) silty SAND :Lig orange-brown,	ine to medium und to subangular (up to 8mm); with ht-brown and	Г		-27 ₁₀₅ - -28 ₁₀₄ -			
	c	CH \from 28.00 m, t \and red high pla CLAY :Dark-gre plasticity, stiff; t	becoming with grey asticity clay (20%) by (trace red), high trace fine to medium 10%): high plasticity			-29103- -30102- -31101-	29.0 to 30.0 n Bentonite pelle sei	et — ►	
		at 33.00 m: Dar	rk-grey (trace red)			-32 ₁₀₀ - -33 99- -34 98-	30.0 to 36.0 n Filter sar backf	nd — 🖌 کُرْش کُرْش 🖌 – bi	
						-35 97- - 3 6 96-			
						-37 95- -38 94-			
						-39 93-			

ient	: V		e Pty I	Ltd	Fi	Proj	ect No	She : 60595		Start Date:	GW2
ojec cati iller ill T	on: B : N	VONBANK anyena Rd lcLeish Drillin lud Rotary	g			Che East				End Date: Location Me Top of Casin Ver. Datum:	21/02/2019 th.:dGPS0.001 g: AHD
ill N	lodel: E	dson 6000 Tr		Nounted	•		-		4/GDA94-54H	Surface:	Topsoil
ill F	luid: V	/ater / Liquipo	bl		Bore Dia.: 150 mm	Pipe	Dia.:	50 mn	ו	Permit No.:	WLE073514
Drill Method	Sample Interval PID (ppm)	Sample ID	Analysed Granhic Log	Classification	LITHOLOGICAL DESCRIPTION	Moisture	Consistency/ Relative Density	Depth (m) Reduced Level (m)	1.0 above grou	m:>	ON DETAILS
				CL	silty CLAY :Brown, low plasticity, soft to firm: low plasticity			0 140-	0.0 to 0.3 Concr	m:	
				CL	CLAY :Orange-brown and brown, medium to high plasticity, stiff: low plasticity			-1			
				SM	sitty SAND :Orange-brown, fine to coarses grained subround, well sorted sand (quartz), partially			-2 139			
				SW	(weakly) cemented SAND :Orange brown and brown, fine to coarses subround, well graded sand; trace silt (<10%)			-3 137-			
				SM	silty SAND : Orange-brown, fine to			136- -5			
				SW	medium grained, subround sand. gravelly SAND :Orange-brown, fine to coarse, well graded sand, fine subround guarz gravel (oxidised,			-6 135-			
Mud Rotary				SP	dark brown), pale grey clay fines (~15%) SAND :Orange-brown, fine to medium grained, subround (quartz)			-7 -7 -8 -9 132- -9 131-			
MudF					from 11.00 m, becoming fine grained from 12.00 m, becoming light yellow-brown mottled orange-brown and grey, fine to medium grained			-10 ¹³⁰⁻ -11 ¹³⁰⁻ -12 ¹²⁹⁻ -12 ¹²⁸⁻			
					from 17.00 m, becoming orange-brown, fine to coarse, poorly graded			-14 ¹²⁷⁻ -15 ¹²⁶⁻ -16 ¹²⁵⁻ -17 ¹²⁴⁻ -17 ¹²⁴⁻ -18 ¹²²⁻ -19 ¹²²⁻ 121-	0.3 to 33.0 Bentonite gr		0.0 to 35.0 m: 50 mm CL18 uPV

ill N	t: / on: [: [ype:] lode]: [WIM Resource AVONBANK Banyena Rd McLeish Drillin Mud Rotary Edson 6000 Tr	g uck			Total Depth:46.00 m	Loge Che East Nort Hor.	ged by cked l ting: hing: Proj/l	y: V by: T 6 5 Dat1	/IGA94/	n th	Top of Ca Ver. Datu	: Meth asing:	AHD Topsoil
ill F	luid: \	Water / Liquipo	bl			Bore Dia.: 150 mm	Pipe	Dia.:	5	50 mm		Permit N	o.:	WLE073514
Drill Method	Sample Interval PID (ppm)	Sample ID	Analysed	Graphic Log	Classification	LITHOLOGICAL DESCRIPTION	Moisture	Consistency/ Relative Density	Depth (m)	Reduced Level (m)	WELL (CONSTRUC	TION	DETAILS
					SW	SAND :Light yellow-brown and red, fine to coarses grained, well graded, subround to ubangular			20 21 22	120				
			•			at 22.00 m: trace dark grey coarse sand at 23.00 m: trace dark grey clay fines			-23	118-				
Mud Rotary				с. 4 6 6 6 6 6 6 6 6 6 6 6 6 6	SW- SM	gravelly SAND :Light yellow-brown, fine to coarse grained, well graded; fine subangular (quartz and ferruginous sandstone) gravel, with silt (10%)			-25 -26 -27 -28	116 115 114 113 112				
MudF			-		SM	sandy SILT :Light yellow-brown, non plastic, fine to medium grained sand, trace (10%) fine gravel			-30 -31	110				
			-		SM	silty SAND :Light yellow-brown, fine to coarse grained sand and dark grey silt fines, trace fine grained subround gravel from 33.50 m, becoming gravel			-32 -33	108	33.0 to 34.0 Bentonite pe			
					GM	content increasing silty GRAVEL .Red and grey, fine to medium grained, subround gravel, grey silt/clay fines, trace fine to coarse grained sand			-36	106	J			
					SC	sandy CLAY :Grey, high plasticity; fine to medium grained sand, trace fine grained subround gravel (<5%)	_		-37 -38 -39	102	34.0 to 41.0 8/16" Filter sa			35.0 to 41.0 m: 50 mm CL18 uPV 0.4mm machine slotted screen
					СН	CLAY :Mottled grey, red and orange-brown, high plasticity, firm to stiff: high plasticity				101				

A=C	MO			Fir	nal				ONITORIN et: 3 of 3	G WELL	GW20
Drill Model	WIM Resource AVONBANK Banyena Rd McLeish Drillin Mud Rotary Edson 6000 Tr Water / Liquipo	g uck Me		Total Depth: 46.00 m Bore Dia.: 150 mm	Logg Cheo East North Hor.	hing:	: 60 : W oy: Tin 61 59 Dat:M)595('ill Dil m Sn 1294 <i>°</i> 95389	006 Ilon nith 1.100 m 98.250 m 4/GDA94-54H	Start Date: End Date: Location Meth Top of Casing Ver. Datum: Surface: Permit No.:	
Drill Method Sample Interval	Sample ID	Analysed Graphic Log	Classification	LITHOLOGICAL DESCRIPTION	Moisture	Consistency/ Relative Density	Depth (m)	Reduced Level (m)	WELL C	CONSTRUCTION	I DETAILS
Mud Rotary			СН	silty SAND :Yellow-brown, fine to medium grained, rounded, indurated CLAY :Dark grey to black, high plasticity, stiff; with fine to medium grained sand (-20%): high plasticity SANDSTONE :Dark grey, fine to medium grained, ferruginous (coffee rock) CLAY :Dark grey to black, high plasticity, stiff: high plasticity at 44.00 m: with sand (-20%) (shells and shell fragments)	2		-41 -42 -43 -44 -45	99- 98- 97- 96-	41.0 to 42.0 Bentonite pel so 42.0 to 46.0 Filter sa back	let →	
							49 50 51 52 53 54 55 56 57 58 59	94 93 92 91 91 90 88 87 86 87 87 86 87 87 87 87 88 87 87 88 87 88 87 88 87 88 87 88 87 88 88			

Drill Model:	WIM Resource AVONBANK Test Pit Crest McLeish Drillin Mud Rotary Edson 6000 Tr Water / Liquipo	g uck	-		Fir Total Depth: 31.00 m Bore Dia.: 150 mm	Proj Logg Chee East Nort Hor.	ect No ged by cked l ing: hing:	y: T by:T 6 5 Dat:N	She 05950 im Sn im Sn 16130 94410	nith nith 6.460 m 04.590 m 4/GDA94-54H	Start Da End Dat Location Top of C Ver. Dat	te: e: n Meth Casing um:	GW2 25/02/2019 26/02/2019 .:dGPS0.001 : 8888.000 mRL AHD Topsoil WLE073514
Drill Method Sample Interval PID (nom)	Sample ID	Analysed	Graphic Log	Classification	LITHOLOGICAL DESCRIPTION	Moisture	Consistency/ Relative Density	Depth (m)	Reduced Level (m)	WELL C 1.0 above groun to 0.0 r Standbi	nd m: —►		DETAILS -0.8 to 0.0 m: 50 mr Standpipe
Mud Rotary				SC CI CH SM SP SM SP-SM SC	silty CLAY :Dark grey, no to low plasticity, soft; trace medium to coarse angular (quartz) sand: low plasticity sandy CLAY :Brown-grey, low plasticity, soft; medium grained, subround to subangular (quartz) sand (20-30%), gap graded CLAY :Light yellow-brown, soft to firm; with fine to medium grained subangular to angular sand (10-20%), poorly graded: medium plasticity CLAY :Light grey and Light brown mottled, high plasticity, stiff to very stiff; trace fine angualr (partially feruginious) sand (5-10%): high plasticity at 7.00 m: silty CLAY: brown grey, medium plasticity, soft; trace fine sand (<5%) silty SAND :Light yellow-brown, fine to coarse subround to angular (quartz) sand, well graded, some slight induration and trace ferruginised SAND :Light grey, fine to coarse grained, subangular, poorly graded (mostly coarse) (quartz) sand, trace silt silty SAND :Light grey, fine to coarse, subangular to angular (quartz) sand, well graded; silt (20-30%), traces of very weakly indurated zones SAND :Light yellow-brown, fine to medium grained, very weakly indurated zones SAND :Light yellow-brown, fine to medium grained, very weakly indurated zones SAND :Light yellow-brown, fine to coarse, subangular to angular (quartz) sand, well graded; silt (20-30%), traces of very weakly indurated zones SAND :Light yellow-brown, fine to coarse, subangular to angular (quartz) sand, well graded; silt (20-30%), traces of very weakly indurated zones SAND :Light yellow-brown, fine to coarse, subangular to angular, well graded, slightly ferruginous at 15.00 m: yellow-brown			1 2 3 4 4 5 6 7 8 9 10 11 11 12 13 14 15 16 17 18 19 10	128 127 126 125 124 123 124 122 122 121	Concre 0.3 to 18.5 f Bentonite gro 18.5 to 19.8 f Bentonite pell se	n:		0.0 to 21.0 m: 50 mm CL18 uPVC

Project: / Location: 7 Driller: N Drill Type: N Drill Model: E	WIM Resource Pty Ltd AVONBANK Fest Pit Crest McLeish Drilling Mud Rotary Edson 6000 Truck Moun Nater / Liquipol	nted Total Depth: 31.00 m Bore Dia.: 150 mm	Logged Checked Easting: Northing	j: 5944104.5 j/Dat: MGA94/GE	Start Date: End Date: Location Metl	25/02/2019 26/02/2019 n.:dGPS0.001 g: 8888.000 mRL AHD Topsoil WLE073514
Drill Method Sample Interval PID (ppm)	Samble ID Graphic Log		Moisture Consistency	Reduced Level (m)	WELL CONSTRUCTION	N DETAILS
Mud Rotary		 SW silty SAND : Yellow-brown, fine to coarse grained, subround to angular, well graded, trace weakly indurated dark-grey fines (mineralised?) and ferruginous at 23.00 m: increasing percentave of black indurated flecks/bands at 25.00 m: dark-brown CL CLAY :Light yellow-brown, low to medium plasticity, with fine grained sand (<5%). Significant contamination from 20m-25m in sample: low plasticity CLAY :Light yellow-brown, low to medium plasticity; trace fine sand: medium plasticity; trace fine sand: medium plasticity, firm; trace fine sand; CLAY lens ~100mm CH CLAY :Dark brown, medium to high plasticity, firm; trace fine sand (<5%): high plasticity at 30.90 m: Dark grey 		118 21 117 22 116 23 116 23 116 24 114 25 113 26 112 27 28 110 29 109	9.8 to 27.0 m: 16" Filter sand 7.0 to 27.5 m: entonite pellet seal 7.5 to 29.0 m: Filter sand backfill 9.0 to 31.0 m: Collapse	21.0 to 27.0 m: 50 mm CL18 uPVC, bell end, 0.4mm

rill Mod	A\ Lo M e: M	IM Resource /ONBANK ongerong Rd cLeish Drillin ud Rotary dson 6000 Tr fater / Liquipc	g ruck			Total Depth:30.00 m Bore Dia.: 150 mm	Logo Cheo East Nort Hor.	ged by cked b ing: hing:	e: 60595 r: Will Di oy: Tim Sr 61276 59416	llon nith 8.480 m 67.440 m 4/GDA94-54H	Top of Ca Ver. Datu	: Meth. asing: ım:	18/02/2019 18/02/2019 :dGPS0.001 8888.000 mRL AHD Topsoil WLE073514
Drill Method Sample Interval	PID (ppm)	Sample ID	Analysed	Graphic Log	Classification	LITHOLOGICAL DESCRIPTION	Moisture	Consistency/ Relative Density	 Depth (m) Reduced Level (m) 	1.0 above grou	m: 🖚		DETAILS 0.8 to 0.0 m: 50 m Standpipe
Mud Rotary					GC SP SM	CLAY :Brown, high plasticity, firm to stiff: high plasticity from 1.00 m, becoming light brown with dark-brown streaks from 2.00 m, becoming light yellow-brown, stiff; trace fine grained sand (<5%) gravelly CLAY :Red, light brown and brown, high plasticity, stiff; gravels are fine grained, subangular (~20%) SAND :Light yellow-brown to pale grey, fine to coarse grained, well graded; with fine grained subangular gravel (!15%) at 9.00 m: red-brown, with silt silty SAND :Pale grey, fine to coarse grained sand; trace fine subangular (quartz) gravel (<10%) from 12.00 m, becoming fine to medium grained sand from 16.00 m, becoming pale grey sand with yellow-brown, fine to medium grained; with fine subroun to subangular (quartz) gravel (~10%) from 19.00 m, becoming fine grained sand			$\begin{array}{c} 1 \\ 133 \\ 2 \\ 132 \\ 2 \\ 131 \\ 3 \\ 131 \\ 4 \\ 130 \\ 4 \\ 130 \\ 4 \\ 130 \\ 4 \\ 130 \\ 129 \\ 6 \\ 128 \\ 6 \\ 128 \\ 7 \\ 129 \\ 6 \\ 128 \\ 129 \\ 6 \\ 128 \\ 129 \\ 6 \\ 128 \\ 129$	0.3 to 20.0 Bentonite gr Standing wa level at 14.54 26/02/20	ter · m —		_ 0.0 to 22.0 m: 50 mm CL18 uPVC

Project: .ocation: Driller: Drill Type: Drill Model:	WIM Resource Pty Ltd AVONBANK Longerong Rd McLeish Drilling Mud Rotary Edson 6000 Truck Mou Water / Liquipol	nted Total Depth: 30.00 m Bore Dia.: 150 mm	Project No: Logged by: Checked by Easting: Northing: Hor. Proj/Da Pipe Dia.:	Will Dillon	Surface:	
Drill Method Sample Interval PID (ppm)	Sample ID Graphic Log	LITHOLOGICAL DESCRIPT	N oisture Consistency/ Relative Density	Depth (m) Reduced L	CONSTRUCTION	DETAILS
Mud Rotary		P-SM silty SAND : Yellow-brown, fine grained, poorly graded at 22.00 m: fine to coaarse graine moderately graded, with fine to coarse grained subangular grave from 24.50 m, becoming yellow-brown, fine to medium grained sand (~20% ferruginous) Plasticity, trace fine to coarse sar (ferruginous): medium to high plasticity, trace fine to coarse sar (ferruginous): medium to high plasticity, stift, trace fine to mediu grained sand (<10%): high plastic	ed, I Ind City	21 22 112 23 111 24 110 24 110 25 109 25 109 26 108 27 107 28 107 28.0 to 28.0 8/16" Filter s 28.0 to 28.4 Bentonite p 29 105 28.5 to 30.0 Filter s	0 m:	22.0 to 28.0 m: 50 mm CL18 uPVC 0.4mm machine slotted screen
				37 97 38 96 39 95 39 95 94		

Appendix D

Groundwater Laboratory Analysis Reports

Appendix D Groundwater Laboratory Analysis Reports



CERTIFICATE OF ANALYSIS

Work Order	EM1904454	Page	: 1 of 8	
Client	: WIM Resource Pty Ltd	Laboratory	: Environmental Division Me	elbourne
Contact	: MICHAEL WINTERNITZ	Contact	: Customer Services EM	
Address	: 201 Elizabeth Street	Address	: 4 Westall Rd Springvale V	IC Australia 3171
	Sydney			
Telephone	: 0467 515 100	Telephone	: +61-3-8549 9600	
Project	: 60595006	Date Samples Received	: 27-Mar-2019 15:00	and the second s
Order number	: 60595006/2	Date Analysis Commenced	: 27-Mar-2019	and the second s
C-O-C number	:	Issue Date	: 08-May-2019 09:54	
Sampler	: BREANA MCCARTNEY		2	Hac-MRA NATA
Site	: Avonbank			
Quote number	:			Accreditation No. 825
No. of samples received	: 9			Accredited for compliance with
No. of samples analysed	: 9			ISO/IEC 17025 - Testing

This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted. This document shall not be reproduced, except in full.

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results

Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QA/QC Compliance Assessment to assist with Quality Review and Sample Receipt Notification.

Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

Signatories	Position	Accreditation Category
Dilani Fernando Kim McCabe	Senior Inorganic Chemist Senior Inorganic Chemist	Melbourne Inorganics, Springvale, VIC Brisbane External Subcontracting, Stafford, QLD
Titus Vimalasiri	Metals Teamleader	Radionuclides, Fyshwick, ACT



General Comments

The analytical procedures used by the Environmental Division have been developed from established internationally recognized procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are employed in the absence of documented standards or by client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing purposes.

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contact for details.

Key: CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society. LOR = Limit of reporting

^ = This result is computed from individual analyte detections at or above the level of reporting

ø = ALS is not NATA accredited for these tests.

~ = Indicates an estimated value.

- Radiological work undertaken by ALS Laboratory Group (Ceska Lipa) under CAI accreditation No. L1163. Report No. PR1935438. NATA and CAI accreditations' are both recognised under ILAC.
- EA010-P: Electrical Conductivity @ 25°C was analysed by manual method (EA010).
- Gross Alpha and Beta Activity analyses are performed by ALS Fyshwick (NATA Accreditation number 992).
- Ionic balances were calculated using: major anions chloride, alkalinity and sulfate; and major cations calcium, magnesium, potassium and sodium.
- ED045G: The presence of thiocyanate can positively contribute to the chloride result, thereby may bias results higher than expected. Results should be scrutinised accordingly.
- EA016: Calculated TDS is determined from Electrical conductivity using a conversion factor of 0.65.
- Sodium Adsorption Ratio (where reported): Where results for Na, Ca or Mg are <LOR, a concentration at half the reported LOR is incorporated into the SAR calculation. This represents a conservative approach for Na relative to the assumption that <LOR = zero concentration and a conservative approach for Ca & Mg relative to the assumption that <LOR is equivalent to the LOR concentration.

Page	: 3 of 8
Work Order	: EM1904454
Client	: WIM Resource Pty Ltd
Project	60595006



Sub-Matrix: WATER (Matrix: WATER)		Clie	ent sample ID	GW20_25/3/19	GW22_25/3/19	QC01_25/3/19	QC02_26/3/19	QC04_26/3/19
	C	lient sampli	ng date / time	25-Mar-2019 00:00	25-Mar-2019 00:00	25-Mar-2019 00:00	26-Mar-2019 00:00	26-Mar-2019 00:00
Compound	CAS Number	LOR	Unit	EM1904454-001	EM1904454-002	EM1904454-003	EM1904454-004	EM1904454-005
				Result	Result	Result	Result	Result
EA010P: Conductivity by PC Titrator								
Electrical Conductivity @ 25°C		1	µS/cm	9780	10600	<1	16500	1
EA016: Calculated TDS (from Electric	cal Conductivity)							
Total Dissolved Solids (Calc.)		1	mg/L	6360	6890	<1	10700	<1
EA065: Total Hardness as CaCO3								
Total Hardness as CaCO3		1	mg/L	936	623	<1	1840	<1
EA250: Gross Alpha and Beta Activit	v							
Gross alpha		0.05	Bq/L	0.36				
Gross beta activity - 40K		0.10	Bq/L	0.44				
EA251: Radium 226 and Radium 228	Activity							
Radium 226	13982-63-3	0.05	Bq/L	0.05				
Radium 228	7440-14-4	0.08	Bq/L	0.09				
ED037P: Alkalinity by PC Titrator								
Hydroxide Alkalinity as CaCO3	DMO-210-001	1	mg/L	<1	<1	<1	<1	<1
Carbonate Alkalinity as CaCO3	3812-32-6	1	mg/L	<1	<1	<1	<1	<1
Bicarbonate Alkalinity as CaCO3	71-52-3	1	mg/L	206	414	<1	102	<1
Total Alkalinity as CaCO3		1	mg/L	206	414	<1	102	<1
ED041G: Sulfate (Turbidimetric) as S Sulfate as SO4 - Turbidimetric	14808-79-8	1	mg/L	690	381	<1	758	<1
			mg/E	050	301	· ·	730	
ED045G: Chloride by Discrete Analys		1	ma/l	2880	3360	<1	5000	<1
Chloride	16887-00-6	1	mg/L	2880	3360		5060	
ED093F: Dissolved Major Cations		÷						
Calcium	7440-70-2	1	mg/L	154	78	<1	211	<1
Magnesium	7439-95-4	1	mg/L	134	104	<1	319	<1
Sodium	7440-23-5	1	mg/L	1500	1880	<1	2530	<1
Potassium	7440-09-7	1	mg/L	28	16	<1	36	<1
EG020F: Dissolved Metals by ICP-MS		0.01					0.01	
Aluminium	7429-90-5	0.01	mg/L	0.01	0.01	<0.01	<0.01	0.01
Arsenic	7440-38-2	0.001	mg/L	0.006	0.007	<0.001	0.003	< 0.001
Boron	7440-42-8	0.05	mg/L	1.25	2.20	<0.05	1.61	< 0.05
Barium	7440-39-3	0.001	mg/L	0.120	0.079	< 0.001	0.114	< 0.001
Beryllium	7440-41-7	0.001	mg/L	<0.001	<0.001	<0.001	<0.001	<0.001
Cadmium	7440-43-9	0.0001	mg/L	<0.0001	<0.0001	<0.0001	< 0.0001	< 0.0001
Cobalt	7440-48-4	0.001	mg/L	0.010	0.003	< 0.001	0.027	< 0.001
Chromium	7440-47-3	0.001	mg/L	<0.001	0.017	<0.001	<0.001	<0.001

Page	: 4 of 8
Work Order	: EM1904454
Client	: WIM Resource Pty Ltd
Project	: 60595006



Sub-Matrix: WATER (Matrix: WATER)		Clie	ent sample ID	GW20_25/3/19	GW22_25/3/19	QC01_25/3/19	QC02_26/3/19	QC04_26/3/19
·	C	lient sampli	ng date / time	25-Mar-2019 00:00	25-Mar-2019 00:00	25-Mar-2019 00:00	26-Mar-2019 00:00	26-Mar-2019 00:00
Compound	CAS Number	LOR	Unit	EM1904454-001	EM1904454-002	EM1904454-003	EM1904454-004	EM1904454-005
				Result	Result	Result	Result	Result
EG020F: Dissolved Metals by I	CP-MS - Continued							
Cerium	7440-45-1	0.001	mg/L	<0.001	<0.001	<0.001	<0.001	<0.001
Copper	7440-50-8	0.001	mg/L	0.003	0.007	<0.001	<0.001	<0.001
Manganese	7439-96-5	0.001	mg/L	0.424	0.052	<0.001	0.717	<0.001
Nickel	7440-02-0	0.001	mg/L	0.015	0.014	<0.001	0.044	<0.001
Lead	7439-92-1	0.001	mg/L	<0.001	<0.001	<0.001	<0.001	<0.001
Selenium	7782-49-2	0.01	mg/L	0.01	0.06	<0.01	<0.01	<0.01
Vanadium	7440-62-2	0.01	mg/L	<0.01	0.02	<0.01	<0.01	<0.01
Zinc	7440-66-6	0.005	mg/L	0.049	0.020	<0.005	0.023	<0.005
Molybdenum	7439-98-7	0.001	mg/L	0.003	0.005	<0.001	<0.001	<0.001
Silver	7440-22-4	0.001	mg/L	0.002	0.002	<0.001	0.002	<0.001
Strontium	7440-24-6	0.001	mg/L	2.42	1.81	<0.001	3.92	<0.001
Thallium	7440-28-0	0.001	mg/L	<0.001	<0.001	<0.001	<0.001	<0.001
Tin	7440-31-5	0.001	mg/L	<0.001	<0.001	<0.001	<0.001	<0.001
Titanium	7440-32-6	0.01	mg/L	<0.01	<0.01	<0.01	<0.01	<0.01
Yttrium	7440-65-5	0.001	mg/L	<0.001	<0.001	<0.001	<0.001	<0.001
Iron	7439-89-6	0.05	mg/L	0.11	<0.05	<0.05	<0.05	<0.05
Bromine	7726-95-6	0.1	mg/L	9.2	5.3	<0.1	17.0	<0.1
G035F: Dissolved Mercury by	FIMS							
Mercury	7439-97-6	0.0001	mg/L	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001
K055G: Ammonia as N by Dis								
Ammonia as N	7664-41-7	0.01	mg/L	0.10	0.79			
K057G: Nitrite as N by Discre								
Nitrite as N	14797-65-0	0.01	mg/L	0.13	<0.01			
		0.01						
EK058G: Nitrate as N by Discre Nitrate as N		0.01	mg/l	0.02	0.10			
	14797-55-8		mg/L	0.02	0.10			
K059G: Nitrite plus Nitrate as								
Nitrite + Nitrate as N		0.01	mg/L	0.15	0.10			
K067G: Total Phosphorus as	P by Discrete Analyser							
Total Phosphorus as P		0.01	mg/L	0.73	0.37			
N055: Ionic Balance								
Total Anions		0.01	meq/L	99.7	111	<0.01	160	<0.01
Total Cations		0.01	meq/L	84.7	94.6	<0.01	148	<0.01
Ionic Balance		0.01	%			<0.01		<0.01
Ionic Balance		0.01	%	8.16	7.95		4.15	

Page	5 of 8
Work Order	: EM1904454
Client	: WIM Resource Pty Ltd
Project	: 60595006



Sub-Matrix: WATER (Matrix: WATER)		Clie	ent sample ID	GW20_25/3/19	GW22_25/3/19	QC01_25/3/19	QC02_26/3/19	QC04_26/3/19
	Cl	ient samplii	ng date / time	25-Mar-2019 00:00	25-Mar-2019 00:00	25-Mar-2019 00:00	26-Mar-2019 00:00	26-Mar-2019 00:00
Compound	CAS Number	LOR	Unit	EM1904454-001	EM1904454-002	EM1904454-003	EM1904454-004	EM1904454-005
				Result	Result	Result	Result	Result
Radionuclides / Activity								
Uranium 238	7440-61-1	0.001	Bq/L	0.107				
Uranium 235	15117-96-1	0.001	Bq/L	0.005				
Uranium 234	13966-29-5	0.004	Bq/L	0.126				
Thorium 232		0.001	Bq/L	0.119				
Thorium 230		0.004	Bq/L	0.024				

Page	: 6 of 8
Work Order	: EM1904454
Client	: WIM Resource Pty Ltd
Project	60595006



Sub-Matrix: WATER (Matrix: WATER)		Clie	ent sample ID	GW14_26/3/19	GW05_26/3/19	GW21_26/3/19	GW18_26/3/19	
	Ci	ient sampli	ng date / time	26-Mar-2019 00:00	26-Mar-2019 00:00	26-Mar-2019 00:00	26-Mar-2019 00:00	
Compound	CAS Number	LOR	Unit	EM1904454-006	EM1904454-007	EM1904454-008	EM1904454-009	
				Result	Result	Result	Result	
EA010P: Conductivity by PC Titrator								
Electrical Conductivity @ 25°C		1	µS/cm	20000	18200	15700	11200	
EA016: Calculated TDS (from Electrica	al Conductivity)							
Total Dissolved Solids (Calc.)		1	mg/L	13000	11800	10200	7280	
EA065: Total Hardness as CaCO3								
Total Hardness as CaCO3		1	mg/L	2150	2040	1840	1310	
EA250: Gross Alpha and Beta Activity								
Gross alpha		0.05	Bq/L		<0.30	0.33		
Gross beta activity - 40K		0.10	Bq/L		0.99	0.62		
EA251: Radium 226 and Radium 228 A	Activity							
Radium 226	13982-63-3	0.05	Bq/L		<0.05	0.08		
Radium 228	7440-14-4	0.08	Bq/L		<0.08	0.10		
ED037P: Alkalinity by PC Titrator								
Hydroxide Alkalinity as CaCO3	DMO-210-001	1	mg/L	<1	<1	<1	<1	
Carbonate Alkalinity as CaCO3	3812-32-6	1	mg/L	<1	<1	<1	<1	
Bicarbonate Alkalinity as CaCO3	71-52-3	1	mg/L	24	35	99	150	
Total Alkalinity as CaCO3		1	mg/L	24	35	99	150	
ED041G: Sulfate (Turbidimetric) as SC			5					
Sulfate as SO4 - Turbidimetric	14808-79-8	1	mg/L	949	983	800	489	
			<u>9</u>					
ED045G: Chloride by Discrete Analyse Chloride	er 16887-00-6	1	mg/L	6610	6400	5140	3970	
	10007-00-0		mg/E	0010	0400	5140	3370	
ED093F: Dissolved Major Cations Calcium	7440-70-2	1	mg/L	260	232	212	220	
Magnesium	7440-70-2 7439-95-4	1	mg/L	365	355	318	185	
Sodium	7439-95-4	1	mg/L	2930	3110	2510	1880	
Potassium	7440-23-5	1	mg/L	34	45	35	1680	
	1440-03-1	1						
EG020F: Dissolved Metals by ICP-MS Aluminium	7429-90-5	0.01	mg/L	0.06	<0.01	<0.01	<0.01	
Arsenic	7429-90-5	0.001	mg/L	0.003	0.024	0.003	0.002	
Boron	7440-38-2	0.05	mg/L	1.54	1.98	1.68	0.80	
Barium	7440-39-3	0.001	mg/L	0.061	0.061	0.111	0.388	
Beryllium	7440-39-3	0.001	mg/L	< 0.001	<0.001	<0.001	<0.001	
Cadmium	7440-43-9	0.0001	mg/L	<0.0001	<0.0001	<0.0001	<0.0001	
Cobalt	7440-48-4	0.001	mg/L	0.012	0.004	0.027	0.001	
Chromium	7440-47-3	0.001	mg/L	<0.001	0.001	<0.001	< 0.001	

Page	: 7 of 8
Work Order	: EM1904454
Client	: WIM Resource Pty Ltd
Project	: 60595006



Sub-Matrix: WATER (Matrix: WATER)		Clie	ent sample ID	GW14_26/3/19	GW05_26/3/19	GW21_26/3/19	GW18_26/3/19	
	Client sampling date / time			26-Mar-2019 00:00	26-Mar-2019 00:00	26-Mar-2019 00:00	26-Mar-2019 00:00	
Compound	CAS Number	LOR	Unit	EM1904454-006	EM1904454-007	EM1904454-008	EM1904454-009	
-				Result	Result	Result	Result	
EG020F: Dissolved Metals by IC	CP-MS - Continued							
Cerium	7440-45-1	0.001	mg/L	0.021	<0.001	<0.001	<0.001	
Copper	7440-50-8	0.001	mg/L	<0.001	0.001	<0.001	0.003	
Manganese	7439-96-5	0.001	mg/L	0.237	0.434	0.706	0.044	
Nickel	7440-02-0	0.001	mg/L	0.020	0.036	0.044	0.003	
Lead	7439-92-1	0.001	mg/L	<0.001	<0.001	<0.001	<0.001	
Selenium	7782-49-2	0.01	mg/L	<0.01	<0.01	<0.01	0.02	
Vanadium	7440-62-2	0.01	mg/L	<0.01	<0.01	<0.01	<0.01	
Zinc	7440-66-6	0.005	mg/L	0.063	0.010	0.022	0.010	
Molybdenum	7439-98-7	0.001	mg/L	<0.001	<0.001	<0.001	0.002	
Silver	7440-22-4	0.001	mg/L	0.002	0.001	<0.001	<0.001	
Strontium	7440-24-6	0.001	mg/L	4.86	4.72	3.79	2.92	
Thallium	7440-28-0	0.001	mg/L	<0.001	<0.001	<0.001	<0.001	
Tin	7440-31-5	0.001	mg/L	<0.001	<0.001	<0.001	<0.001	
Titanium	7440-32-6	0.01	mg/L	<0.01	<0.01	<0.01	<0.01	
Yttrium	7440-65-5	0.001	mg/L	0.003	<0.001	<0.001	<0.001	
Iron	7439-89-6	0.05	mg/L	3.68	4.56	<0.05	<0.05	
Bromine	7726-95-6	0.1	mg/L	22.5	22.5	16.8	12.7	
EG035F: Dissolved Mercury by	FIMS							
Mercury	7439-97-6	0.0001	mg/L	<0.0001	<0.0001	<0.0001	<0.0001	
EK055G: Ammonia as N by Disc	crete Analyser							
Ammonia as N	7664-41-7	0.01	mg/L	0.10	0.05	0.04	0.15	
EK057G: Nitrite as N by Discre								
Nitrite as N	14797-65-0	0.01	mg/L	<0.01	<0.01	<0.01	0.02	
EK058G: Nitrate as N by Discre								
Nitrate as N	14797-55-8	0.01	mg/L	<0.01	<0.01	0.02	0.01	
EK059G: Nitrite plus Nitrate as								
Nitrite + Nitrate as N	N (NOX) by Discrete Ana	0.01	mg/L	<0.01	<0.01	0.02	0.03	
			<u> </u>					
EK067G: Total Phosphorus as I Total Phosphorus as P	P by Discrete Analyser	0.01	mg/L	0.15	0.19	0.65	0.08	
		0.01	iiig/E		0.13	0.00	0.00	
EN055: Ionic Balance		0.01	mog/l	207	202	464	425	
Total Anions		0.01	meq/L	207	202	164	125	
Total Cations		0.01	meq/L	171	177	147	108	
Ionic Balance		0.01	%	9.36	6.46	5.41	7.18	

Page	: 8 of 8
Work Order	: EM1904454
Client	: WIM Resource Pty Ltd
Project	: 60595006



Sub-Matrix: WATER (Matrix: WATER)	Client sample ID			GW14_26/3/19	GW05_26/3/19	GW21_26/3/19	GW18_26/3/19	
	Cl	ient sampli	ng date / time	26-Mar-2019 00:00	26-Mar-2019 00:00	26-Mar-2019 00:00	26-Mar-2019 00:00	
Compound	CAS Number	LOR	Unit	EM1904454-006	EM1904454-007	EM1904454-008	EM1904454-009	
				Result	Result	Result	Result	
Radionuclides / Activity - Continued								
Uranium 238	7440-61-1	0.001	Bq/L		<0.001	0.033		
Uranium 235	15117-96-1	0.001	Bq/L		<0.001	0.002		
Uranium 234	13966-29-5	0.004	Bq/L		<0.004	0.044		
Thorium 232		0.001	Bq/L		<0.001	0.058		
Thorium 230		0.004	Bq/L		<0.004	0.019		